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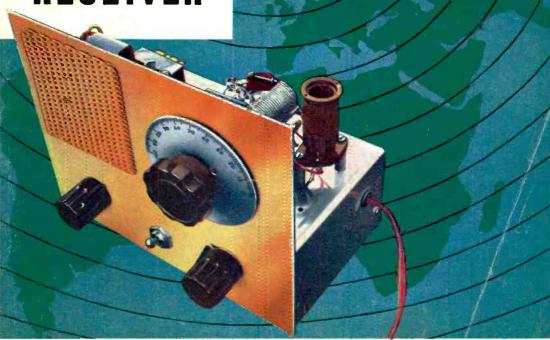


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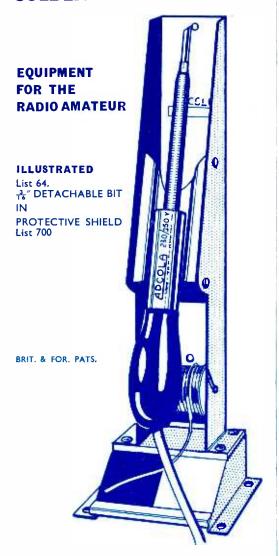
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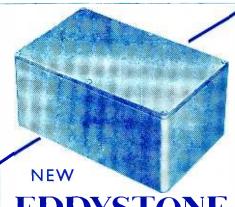
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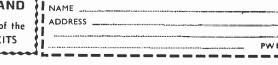
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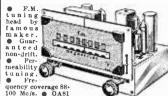
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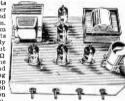
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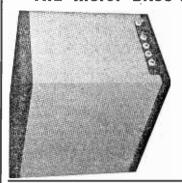
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ALL RECEIVERS AND AMPLIFIERS Using two MICRO-ALLOY TRANSISTORS the Sinclair Micro-Injector Using two interest that the state of the sta

rapidly found. The sinciar Micro-Injector is powered by a 6d, standard battery which will last for about 6 months. Its size is $1_{1/2}^4 \times 1_{2/2}^3 \times 1_{2/2}^4 \times 1_{1/2}^4$ excluding the probe which is $2_{1/2}^4$ on by far the smallest instrument of its kind available. Assembly is extremely simple and will take even a beginner only half an hour. Clearly illustrated building instructions are provided together with operating instructions. rapidiv found.

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OUTPERFORMS AMPLIFIERS 20 TIMES LARGER

This fantastically small, powerful amplifier is smaller than a 3d-piece. With a frequency response from 30 to 50.000 $c/s \pm 1$ dB and power gain of 60dB (1.000,000 times) it becomes a valuable tool in the hands of the keen experimenter as well as providing an excellent sub-ministure hi-fi amplifier with an output suitable for any earpiece or even loudspeaker. With MAT Transistors, brand new micro-ministure quality components and micro-printed circuit. The uses to which this unique amplifier can be put are almost beyond count. Circuitry details are included showing how to use it with high or low impedance inputs, in radio, etc., etc.

Consumption from 0.4 mA at 1.3 v. to 1 mA at 9 volts.

Will drive ANY earpiece or even a loudspeaker.



28/6

Requires no special tools for building.



circuit showing with low and high impedance pick-ups, microphones, tapeheads, in transmitter circuits, as a mono or stereo hi-fi system,

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MAT 100 High gain low level type

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8/6 type
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This new Sinclair transistor, only \(\frac{1}{2} \) high \(\frac{1}{2} \) dia., is specially designed for F.M. and T.V. applications and for V.H.F. and U.H.F. transmitters and receivers. by the alloy-diffused process, the ADT.140 has a typical alpha cut-off frequency of 400 Mc/s. Power gain is 15dB at 100 Mc/s and 9dB at 200 Mc/s.

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Will produce a perfectly clean half walt of audio power even from very low output sources such as low-impedance tape heads, pick-ups and microphones. Ready built and uncon-ditionally guaranteed.

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CIRCUIT—5 matched transistors and temperature compensating diode in a transformerless complementary-symmetry configuration.

POWER OUTPUT—500 mW undistorted into 15 ohms.

SENSITIVITY—0.5 mV.

POWER GAIN—80 dB (100 million times).

FREQUENCY RESPONSE—50 c/s to 20 kc/s ±3dB.

SIZE—2½ x 1½ x ½in.

POWER REQUIREMENTS—10 mA quiescent and 150 mA peak from 9V. battery or power supply.



and still they write!

With each post we get more and more constructors writing to us about the "Slimline". Here's a user who took his to Europe.

HOMER GREEN BUCKS 6.9.63

Dear Sirs, I took the "Slimline" to Paris and to Faentarrabia near Irun in Northern Spain.

Spain.
In Paris we received three French
In Paris we received three French
Stations and Radio Luxembourg at
excellent strength.
In Fuenterrabia we could get a Spanish
station, two or three French stations—
and on one evening the LIGHT PROGRAMME nearly 900 miles away.
In San Sebastian which we visited
one day, the local station was booming
in. We are delighted with the present
performance of the set. I would like
a Sinclair Micro Amplifier and enclose a Sinclair min. cheque for 28/6. With thanks, a Sinclair Micro Amplifier and enclose

Yours sincerely, F.H.R. Aldred.

TAPE RECORDER USERS NOTE

The "Slimline" is unequalled as a radio jack and can be plugged into ANY tape recorder by substituting a plug and lead for the earpiece. Its power and sensitivity are deal for this purpose.

NOW IS THE TIME TO BUILD YOUR SINCLAIR SLIMLINE.

Small enough to conceal in one hand, it gives choice of British and European programmes with staggeringly good quality and selectivity. Building is easy and interesting, and as well as providing superb listening through the earpiece, the "Slimline" makes a wonderful radio jack too.

- * NEW improved solid dielectric tuning capacitor
- * FULL coverage of medium waveband
- ★ USES Micro-Alloy Transistors throughout (MATs)
- * EXTREMELY robust construction
- * TRUE high-fidelity performance with quite incredible volume and quality of reproduction
- * EXTREMELY SENSITIVE—pulls in literally dozens of continental stations right across the band
- ★ IDEAL for use in car or train where tremendous volume is really valuable
- ★ IDEAL as a radio jack for tape recorders, etc.
- ★ COMPLETELY self contained; uses internal ferrite rod aerial and a PP5 battery
- * ELEGANT royal blue case with gold trim and calibrated dial

Size 215 x 115 x 3in. Comprises brand new sub-minia-Comprises brand new sup-minia-ture components, printed circuit board, genuine MAT transistors, case, featherweight quality ear-piece and well illustrated easily followed instructions.

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checked and guaranteed		ranteed	MH4 3/6 ML4 4/-	TT15 80/- TTR31 60/-	2A3 5/- 2A5 6/-	6C4 2/6 6C5G 4/-	6Y6G 6/- 6.30L2 10/-	41MP 4/- 53A 7/6	6073 7/- 6120 4/-
\/A	1 1/ 5		ML6 6/-	TZ20 16/-	2A6 7/-	6C6G 3/-	6Z4 5/-	58 6/-	6516 8/-
I VA	LVE	.5	MS/PEN 6/- N78 12/-	TZ05-20 4/- U12/14 8/-	2C26 3/- 2C26A 3/-	6C8G 3/- 6CH6 5/-	7B7 7/6 7C5 7/-	59 6/- 75 5/6	7193 1/9 7475 3/-
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ARP3 3/- E1	1524 12/6	EL35 5/-	PCC84 6/6	U801 20/- YABC80 7/-	2X2 3/- 3A4 4/-	6F8G 5/- 6F12 4/6	8D2 2/6 9D2 3/-	84 8/- 85A2 7/6	C.R.
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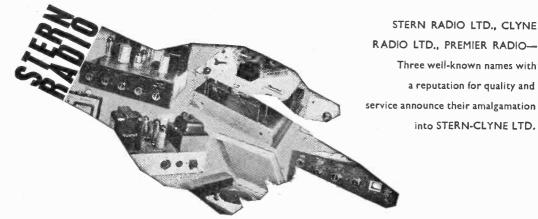
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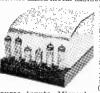
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Aluminium Chassis, 18 s.w.g. Plain undrilled. 4 sides, riveted corners, lattice fixing holes, 24in. sides, 7 x 4in., 4/6; 9 x 7in., 5/9; 11 x 7in., 6/9; 13 x 9in., 8/6; 14 x 11in., 10/6; 15 x 14in., 12/6. Aluminium Panels, 18 s.w.g., 12 x 12in., 4/6; 14 x 9in., 4/-; 12 x 8in., 3/-; 10 x 7in., 2/3; 8 x 6in., 2/-.

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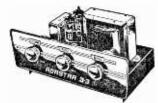
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x 7 in. 17/6;
x 7 in. 17/6;
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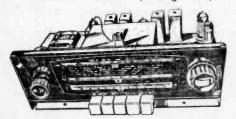
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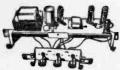


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(6/- Carr.) Brand new 2002/240 A.C. mains.

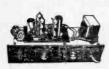
Bass, trebie and vol. controls.

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12 x 3 y x 3 in. With o.p. transle
13 y s x y x 3 in. With o.p. transle
14 y screwed to chassis) may be removed and used as "flying penel"

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The Show That Never Was

N the absence of the customary Radio Show at Earls Court this year, many companies in the radio/TV industry held their own private exhibitions for the trade, primarily retailers and wholesalers. This resulted in the extraordinary situation of something like 30 separate shows of varying size, scattered

mainly around the Central London area.

The formidable task of "doing the rounds" was somewhat alleviated by the sheer novelty and by the exotic experience of visiting a galaxy of plushy suites in such buildings as the London Hilton, the Carlton Tower, the Savoy, the Mayfair, the Cafe Royal, etc. This was certainly a contrast to the rather stolid utilitarian exhibition buildings at Earls Court which even the most colourful displays never seem to completely disguise.

It was quickly obvious from a grand tour of the individual shows that the trade was turning out in force, and organisers expressed delight (and some surprise) that attendance was so far in excess of expectations.

The manufacturers were also pleased that the overall cost of mounting their exhibitions was considerably lower than that necessary for a normal Radio Show, with the added advantage of more comfortable surroundings, more space and much greater

So, from the industry's point of view, the experiment was successful on several counts: costs down, order books full, a more comfortable and a shorter show. But what of the public, who were denied their annual exhibition this year?

Some manufacturers consider that the impact of the public at the Radio Show on sales is small. They reason that since most prospective purchasers are content to be guided by the advice of their local dealers in the choice of a new set, the main task is to get the products into the dealers' shops. The projection of any 'image" or the creation of public demand can best be achieved by planned advertising campaigns.

There is, of course, more than a grain of truth in this and it is probably true to say that only a fraction of the expense involved in exhibiting at the Radio Show is ever offset by sales resulting directly from any demand created at that Show.

And herein, of course, lies the dilemma which caused the cancellation of the Radio Show this year. There has been for years a strong case for a short period trade-only show, with perhaps a different exhibition aimed directly at the public. But it is obvious that here again we are in deep water.

No doubt the industry and the exhibition organisers have already given this problem much thought and will continue to do so. The Radio Show is being resumed again next year under one roof and we hope that in everybody's interest a formula will be found to reconcile the requirements of both trade visitors and the general public. In any event, we shall almost certainly see some changes in the 1964 Radio Show.

Our next issue dated December will be published on November 7th



NEWS AT HOME AND ABROAD

Electrical Engineers Exhibition

AFTER having taken and allocated all available floor space at Earls Court, London, for the Electrical Engineers Exhibition, the organisers have had to partially replan the layout to accommodate extra stands since the demand for exhibiting space has been so great.

To be held from 18th to 25th March, 1964, it will be the only exhibition of its kind in the world that year and, along with the increased number of British exhibitors, many European and other overseas countries will be represented, including 12 from Germany.

TRANSISTORS FROM SOUTH AFRICA

ALREADY South Africa's leading manufacturer of long distance telephone transmission equipment, Standard Telephones and Cables (Pty) S.A. Limited (a subsidiary of the British Firm) will commence manufacture of silicon epitaxial planar transistors at its factory at Boksburg.

near Johannesburg, next year.

An agreement between the the Boksburg company and South African government has been reached for the local manufacture of these components, now that the establishment of a South African plant is justified.

O'N July 20th, 1897, the "Wireless Telegraph and Signal Company Limited" was officially registered in London as a

limited company; total assets £100,000. On the board of directors of this new company was one Guglielmo Marconi-famous pioneer of wireless transmission. In March, 1900, the name of the company was changed—by general consent of the shareholders—to "Marconi's Wireless Telegraph Company Limited".

This, then, became the title under which the world's first wireless manufacturing company was to advance, in the first sixty-odd years of the twentieth from a relatively small £100,000 firm exploiting Guglielmo Marconi's patented methods of wireless transmission. to the international organisation it is today, selling electronic equipment to practically every country in the world.

Now, sixty-six years after the company's inception, the name has once again been changed, the widening scope of the products being produced rendering its former title obsolete. The name of the firm's prime mover will not be forgotten, however, when new equipment manufactured under the new title of "The Marconi Company Limited" reaches its customers the world over.

Congress Tapes

AT one of the largest inter national congresses ever hel in the U.K., the Tannoy group o companies made use of four new RE 301 professional tape recoi ders, recently purchased fror EMI Electronics Limited. Thirty three hours of the congress wer recorded on these machines a the Royal Albert Hall, Londor where the congress was held These recordings were made i two languages, and after suitabl editing and copying, tapes of th highlights of the congress, si hours in length, were distribute to 56 different countries. Later after further editing, three-hou tapes were made available fo distribution throughout world

New V.H.F. Relay Station for Sheffield

INTIL recently v.h.f. sound transmissions in the Sheffield are originated solely from the BBC's Holme Moss station, which because of the hilly nature of the surrounding country, did no provide total coverage of the area. Now, however, another 240,00 listeners in Sheffield will be able to receive v.h.f. transmission from the new Tapton Hill relay station which recently began transmitting the North-of-England. Home Service, the Ligh Programme and the Third Programme on 94.3Mc/s, 89.9Mc/s and 92-1Mc/s respectively.

All transmissions from the new station will be horizontall

polarized.

CRITICAL STAGE OF COMMONWEALTH TELEPHONE CABLE

THE first week of September saw a critical stage in the laying of the Commonwealth telephone cable-Pacific Section. Two cable-laying ships, the HMTS "Monarch" and the C.S. "Retriever" (of Cable and Wireless Limited) faced the task of laying the cable through the Murray Fracture Zone, which is approximately 700 miles north of Hawaii and is the deepest point of the lay between Port Alberni (Vancouver) and Hawaii. Here the ocean is almost 3\frac{1}{4} miles deep and for 60 miles the crews of the ships had to contend with uneven ocean bottom.

However, with yet another part of the mammoth operation over, the forecast looks favourable for the opening of the 8,700 mile cable telephone service linking Britain, Canada, New Zealand and Australia, in December.

Radio Communications Show

THE main feature of the 1963 International Radio Communications Exhibition will be, appropriately enough for this the Golden Jubilee Year show, a display of amateur equipment from 50 years ago, right up to present-day gear.

Every day throughout the show, which will last from October 30th to November 2nd, The Radio Society of Great Britain (the organising body of the exhibition) will be transmitting and

receiving on amateur bands under the call signs GB3RS and GB3VHF. Many hundreds of radio amateurs from all parts of Britain are expected to visit the Seymour Hall (Seymour Place,

Equipment for Ghana

IN Ghana, where Marconi v.h.f. radio equipment has provided the main trunk telephone services for many years, a new multichannel radio relay system, using the same type of equipment, will shortly be in operation, linking the country's capital, Accra, with the new Atomic Research Institute at Kwabenvan.

An ultimate total of 48 telephone channels will be carried by Marconi HM.100 equipment between the two centres.

Marble Arch, London) during the time of the show, where displays, competitions, demonstra-tions, etc., will provide much interest and amusement for all enthusiasts.

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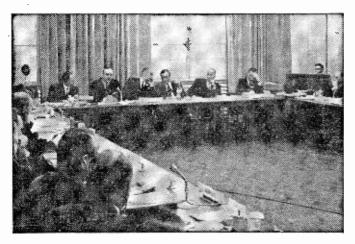
As usual, the armed services will be exhibiting along with the G.P.O., but for the first time, this year the BBC has taken a stand.

Amateur television equipment will amongst the displays, with demonstrations of cameras, film and mobile equipment.

With many other interesting exhibits, visitors to the show can look forward to a very memorable occasion.

INTERPRETATION SOUND SYSTEM

OVERSEAS delegates meeting in the new conference room of the National Coal Board at Hobart House, London, are able to listen to speeches in their own language over a sound system for simultaneous interpretation, manufactured, and recently installed, by Trix Electronics Limited. The installation allows anyone in the room to hear either the spoken address or an interpretation in one of two other languages.



The new conference room at Hobart House, the headquarters of the National Coal Board, where a Trix interpretation sound system has recently been installed.

I.E.E. President

ON 1st October, Sir Albert Mumford, K.B.E., took office as president of the Institution of Electrical Engineers for the session 1963/64. Sir Albert, who is Engineer-in-Chief of the Post Office, was made Knight Commander of the Order of the British Empire in the 1963 Birthday Honours List.

The three I.E.E. division chairmen also elected are; Dr. R. C. G. Williams, Mr. C. D. Wilkinson and Dr. J. R. Mortlock.

RADIO BROADCASTS FOR ADEN

RADIO broadcasts for schools are now taken for granted in the U.K., but for Arab students in Aden, the series of programmes being transmitted by the Aden Forces Broadcasting Association from R.A.F. Khormaksar covering G.C.E. subjects, is proving a worth while addition to their official studies. These weekly broadcasts are being transmitted on an experimental basis, as a prelude to a formal course of study which it is hoped to start in the future.

Beginner's SHORT WAVE TWO

The Blueprint given away free in this issue provides all the diagrams necessary to build this receiver. Newcomers to radio construction will find this design to be straightforward and inexpensive, thus making it an ideal introduction.

BY F. G. RAYER

THIS receiver uses a 954 acorn valve as detector, followed by a 12AT7 twin triode as two-stage audio amplifier. It is constructed on a 7in. x 4in. x 2½in. chassis, and includes a mains powerpack and 2½in. diameter loudspeaker. The panel is approximately 6in. x 7½in. The whole receiver is thus of small size.

The circuit is shown in Fig. 1. The receiver may be used over all frequencies from 1·2Mc/s to 100Mc/s (250-3m). Efficient results are of course obtained at lower frequencies than 1·2Mc/s, but the small size of VC1 makes waveband coverage rather small. For general short wave listening, a single coil covering about 14-40 metres (22-7Mc/s) will be very convenient. A second coil will allow coverage to 2·5Mc/s (120m). Such a pair of coils will allow many of the most useful bands to be tuned. Regeneration is obtained by means of the cathode tap 2 on the coil L1, and is controlled by the potentiometer VR1.

VR2 is the audio gain control, or volume control. The second triode section of the 12AT7 drives the loudspeaker through the matching transformer T1 and provides quite a reasonable output. For the power pack, two small metal rectifiers are employed for full-wave rectification, and complete isolation of the receiver from the mains, is effected by the power transformer T2.

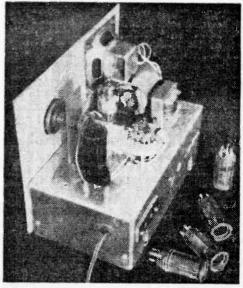
power transformer T2.

In a receiver of this type, the layout of components in the audio stages and power supply circuit is of little importance. In the detector stage, however, wiring must be short and direct, and construction must be rigid. A valve rectifier, such as 6X4, could be used, and also a larger loud-speaker, if so desired.

Chassis Layout

This is shown in Fig. 2. VC1 is fixed to a stout bracket, so that a ball drive may be added. Tuning is quite critical, and a 2in. dia. knob is recommended. The lug on the drive is bolted to the panel. The drive is fitted with a 0-100 or 0-180 dial, or a pointer, which can be read against scales drawn on card attached to the panel.

The coil holder is mounted about \$\frac{1}{4}\$ in. above the chassis, using long bolts with extra nuts. or spacing sleeves for this purpose. Coil formers and holders other than those listed may be fitted, or a single coil, permanently wired. There is no need for the coils to be of the diameter given, and other



A rear view of the receiver, with some spare coils.

numbers of turns and gauges of wire can be perfectly satisfactory. Changing the diameter or windings will naturally modify the waveband covered, but provided smooth regeneration is obtained, there will be no loss of efficiency.

It is quite feasible to wind coils on old valve bases, or on paxolin tubes attached to old bases. Larger plug-in coils are also available from some suppliers, and can generally be used, if to hand. Fig. 4(d) shows the underside of the coils, and

Fig. 4(d) shows the underside of the coils, and pin connections. The tuned winding is between pins 1 and 3, pin 3 being earth. All cathode taps are made on this winding, at point 2. The remaining winding is for aerial coupling, the aerial being connected via C1 to socket 4. The remaining end of the aerial coupling winding is taken to pin 3.

All the coils are made in the same way, except for the number of turns and gauge of wire. If valve bases or other coils are used, the holder is

selected to suit, and appropriately wired, so that any coil can be inserted.

On the plug-in coils listed, the following numbers of turns may be used, the ranges specified being approximate.

6.75-22Mc/s 16 turns 30s.w.g., tap at \(\frac{3}{4}\) turn.

Aerial coupling, five turns.

2.5-7.5Mc/s 50 turns 32s.w.g., tap at $1\frac{1}{2}$ turns. Aerial coupling, 15 turns. 1.2-4Mc/s 100 turns 34s.w.g., tap at 2 turns.

Aerial coupling 20 turns. 14.5-50Mc/s $5\frac{1}{2}$ turns 30s.w.g., tap $\frac{1}{3}$ to $\frac{1}{2}$ turn.

Aerial coupling two turns.

Approx. 40-100Mc/s 2½ turns 20s.w.g. double spaced, tap at ½ turn. Aerial coupling one turn.

The two larger coils have turns side by side. Other coils are on threaded formers, with 21 turns per inch. Aerial windings are near the tuned windings, as in Fig. 4(d). The highest frequency range is with VC1 in the half-closed position (75pF).

Acorn Valve

Pin connections for the acorn valve are shown in . Fig. 4(a), the valve being viewed from the anode (long) end. The valve is mounted over a 1in. diameter hole, so that the grid pin is on top, as in Fig. 2, and the anode pin under the chassis, as in Fig. 3.

The valve can be mounted satisfactorily by soldering wires directly to the pins, provided care is taken to avoid breaking the glass seal. Wires must be soldered only to the extreme tips of the pins, and the iron must be at full temperature, and must be removed promptly when the connection has been made.

If a valveholder is used, grid and anode connections may be soldered or clipped on. The leads from R1 and C2 to the grid pin should be extremely short, to avoid hum. If the outside foil of C2 is marked, take this end to VC1.

Loudspeaker and Panel

The panel may be painted, or left clear. It is held to the front runner of the chassis by the

swith and the two potentiometers.

A clip holds the twin capacitors C9 and C10 to the chassis, and if this component does not have a metal can forming the negative connection, and in contact with the chassis, a lead should be added from negative to chassis.

The loudspeaker is just high enough to clear the capacitor, and has a matching aperture in the panel. It is secured with countersunk 6B.A. bolts. A square piece of expanded metal loudspeaker fret is then cemented to the panel, over the

aperture.

Below the Chassis

Wiring and components are shown in Fig. 3. The two small, contact cooled rectifiers MR1 and MR2 are bolted to one side runner. The Mains transformer wiring should be checked as follows:

Primary to mains, via on/off switch. One 6.3V tag and centre tap of h.t. winding to chassis. Remaining 6.3V tag to tag 9 of the 12AT7 holder, and 954 heater. The h.t. tag to negative on one rectifier. Second h.t. tag to negative on second rectifier,

A tag strip with two insulated tags will be convenient to anchor the mains leads, which pass through a grommet in the chassis. Current is best drawn from a plug fitted with a low rating fuse. The receiver chassis should be earthed.

Various points marked "MC" in Figs. 2 and 3

are all soldered to tags which are bolted securely to the chassis. The negative ends of C5 and C8

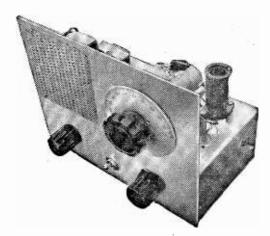
must be taken to the chassis.

Operating

A regenerative receiver of this type is extremely sensitive, provided regeneration is correctly adjusted. If regeneration is not use correctly, only powerful European and similar stations will be heard.

When VR1 is slowly rotated so as to increase the 954 screen grid voltage from zero, a point will be found where oscillation begins. This oscillation is audible if a station is nearly tuned in, and will be heard as a whistle, or audio tone, which changes in pitch as tuning is adjusted. For maximum sensitivity, regeneration is kept at the point where such oscillation just fails to arise. In these conditions, extremely weak signals may be picked up.

Regeneration and tuning are critical, with the high frequency coils, and when receiving weak signals. With the lower frequency coils, and when tuning in stronger transmissions, the setting of VR1 is less important. For powerful stations received without interference, VR1 may be turned back somewhat. But in more difficult reception



The finished receiver.

conditions, VR1 is maintained near the oscillation point, as described, because this increases selectivity, and volume is reduced by VR2, if needed.

If regeneration is too violent and abrupt, with any coil, this shows that the tapping 2 needs to be slightly nearer the earthed end of the coil 3. Aerial loading influences results, and if the aerial is at all long, C1 should be reduced in capacity. This can be done by fitting a 30pF or 50 pF trimmer in this position. For indoor and other short aerials, C1 may be as shown.

SHORT WAVE

RECEIVING

AERIALS

Details for planning and constructing S.W. aerials to suit restricted environments are given in this article

by A. W. Mann

A LTHOUGH highly efficient short-wave receivers are commonplace today, many are used in conjunction with aerials of comparatively low efficiency. This is, however, often no reflection on the designers or operators but is due to lack of space for outdoor erection of recommended types exactly to specification. But there are many ways in which this problem can be resolved and ample scope for originality.

Vertical aerials are used by many short-wave broadcasting authorities throughout the world and Fig. 1 shows a vertical type receiving aerial which can be erected at a comparatively low cost. All that is required is a pole of 2in. or 2½in. square section, an ex-Services type 8ft two-section whip aerial and rubber mounting base with three beehive type insulators and sufficient wire for the down lead.

Note the platform dimensions: 8in. x 6in. x 1in., fitted to the top of the pole, and the method of mounting. Use wood screws in preference to nails. The dimensions should be adhered to as the base flange of the aerial mounting is 8in. diameter. If smaller insulators than the type recommended are to hand they could be used if mounted on 1½in. wooden blocks nailed to the nole.

If insulated wire is used for the downlead do not fix it to the pole by means of insulated staples, otherwise considerable damping will result.

As vertical aerials are omnidirectional, excellent results may be expected providing that they are erected at a sufficient height. The author strongly recommends this type of aerial for use with receivers incorporating one or more r.f. stages.

In the case of regenerative receivers with no r.f. stage, a rigid copper rod is preferable to a rubber-

base mounted whip to avoid instability due to swaying in the wind. This does not apply to superhets.

Tuning the Aerial

It is generally appreciated that a tuned aeria system is more efficient than an untuned one an in addition improves the signal-to-noise ratic Fig. 2 shows a pi-type aerial tuner using a multi tapped coil tuned by two variable 200pF capacitors, the taps being selected by a rotary switch. The tuning coil consists of 25 turns of 20 gaugitinned copper wire spaced one diameter of the wire and wound on a lin. diameter former.

This type of tuner should be built into a meta box. Efficient screening is essential in order to avoid direct pick-up by the coil winding, and to sharpen the tuning.

Tuning Procedure

First tune in a signal on the receiver and their rotate the aerial tuner controls to obtain a peak signal while trying different tappings. The optimum tapping is the one at which readjust ment of the tuning controls produces the loudes signal and lowest noise level.

The peak points, which are more or less constant for a given band, are not the same for al

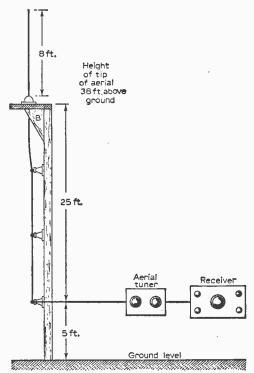


Fig. 1: An inexpensive but efficient vertical aerial.

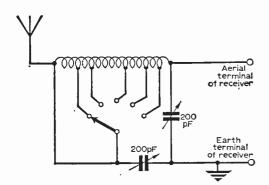


Fig. 2: A pi-type aerial tuner using a multi-tapped coil.

bands, and changing from one band to another calls for retuning of the aerial and some adjustment of the tapping points.

Once the peak points of the different bands have been found, the dial readings and tapping points can be logged for future reference. While additional tuning controls are generally to be avoided if possible, in the case of aerial tuners the advantages far outweigh the disadvantages.

Other Aerial Tuners

At Fig. 3 another very simple yet efficient aerial tuner is outlined. This consists of 26 turns of 14 gauge tinned copper wire spaced 1/8 in. between turns on a 1½ in. diameter former. Tapping points are made by spring clips, later to be replaced by a suitable switch.

With this particular tuner no difficulty should be experienced. It is necessary only to set the aerial tuning dial at zero, tune in a signal on the receiver, then tune the signal to maximum volume with the tuner. Try different tappings, then retune the aerial. At one point on a particular turn the actual peak point will be found.

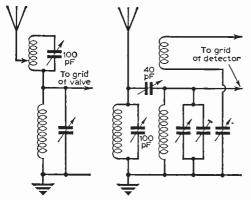


Fig. 3 (left): Another simple aerial tuner. Fig. 4 (right): This method of tuning uses a duplicate set of plug-in coils.

This procedure should be followed on all bands and the tapping points and dial readings noted. It should be remembered that when using tapped coils and spring clips in the initial tests, it is not sufficient to select merely the correct turn on the coil, but also the correct part of the turn from which to take a permanent tap to a rotary switch. This particular form of aerial tuner is ideal for use with receivers of the regenerative type.

Fig. 4 shows a method of aerial tuning in which a duplicate set of plug-in coils is used. This can also be used as an additional selectivity device and wave trap and is suitable for use with regenerative receivers. If used in conjunction with plug-in coils of identical type and make to those in the receiver no difficulty will be found in tuning to resonance. In the case of this and the series tuner of Fig. 3 a slight backing-off from the resonance point will assure stability.

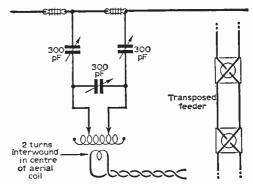


Fig. 5: This tuner is designed primarily for open wire or transposed feeders.

The aerial tuner shown at Fig. 5 is designed for aerials with open wire or transposed feeders. Although it can be used with twisted flex feeders, tuning is rather difficult.

Indoor Directional Aerials

It sometimes happens that the erection of a good outdoor receiving aerial is impracticable or forbidden. The problem is to decide what form an indoor aerial should take.

If a criss-cross roof space arrangement is used with a single wire down lead, the chances are that the latter will be longer than the aerial if the receiver is located in a downstairs room, and furthermore will be heavily damped due to its proximity to walls.

The foregoing remarks are based on personal experience and is the reason why many really sensitive receivers give a below-average performance when used under such conditions. If, however, it is possible to arrange the down lead away from the wall a marked improvement will result. Even so, such indoor aerials are of comparatively low efficiency.

With the foregoing considerations in mind readers should consider the erection of a dipole type, providing that each span can be at least 20ft long.

In many instances however, that will be impossible in the average roof space. However,

each span can be bent as shown at Fig. 6 and Fig. 7. The spacer shown at Fig. 8 is of plastic or other insulating material fitted with two terminals.

minals.

Plastic-covered electrical flex may be used for the transmission line and the switching over from one aerial to the other may be achieved via a relay or a double-pole, double-throw switch. The arrangement shown at Fig. 6 was fully described as relay switched by the author in *Practical Wireless* some years ago.

The use of a single dipole of the forms described

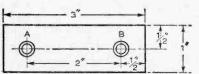
Twisted PVC flex

B

South hook

South hook

Figs. 6 (above) and 7 (right): Show how indoor aerials may be bent to be accommodated in limited space. Fig. 8 (below): Shows the spacer.



here is not recommended for indoor use as it is very directional. This type of aerial is only recommended when arranged as described due to its broadside directive properties. This means that for east-west reception the aerial must be run north to south

and for north-south reception east to west.

If arranged as suggested the twin dipoles will provide world-wide coverage. Anyone using a receiver fitted with an S meter will find that tests using alternative aerials on a given signal will show a marked increase or decrease in signal strength, sometimes from 4 to 5 S points.

During the past 18 months the author has used the aerial shown at Fig. 6 exclusively in conjunction with a Senior National H.R.O. Using the eastwest aerial a particular amateur band could appear to be more or less dead, whereas switching to the north-south aerial produced strong signals from some unexpected sources. This shows that although the H.R.O. is of high sensitivity the

aerials are also very efficient. For some years this particular arrangement has also been used with the RII55A and RIII6A with gratifying results.

General Arrangements

Let us examine the sketch at Fig. 6 in detail From A to D is a single wire, as is B to C, E to F and G to H. In Fig. 7 we have single wires A to B, C to D, E to F and G to H. Two separators fitted with terminals or suitable sockets and plugs are required, details of which are given in Fig. 8 Stranded insulated aerial wire should be used and the aerial system should be supported by small brass hooks.

A Horizontal U Aerial

Where a short-wave receiver is used in a separate room the aerial arrangement shown at Fig. 9 provides scope for experiment if suspended above the receiver and between the end walls,

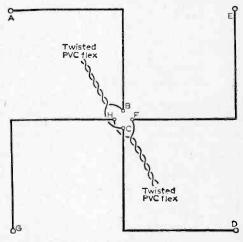


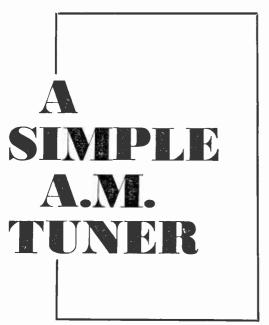
Fig. 9 (below): An aerial suitable for assembling in a room.

Downlead Afterminals Bell terminals Bell terminals

The down lead will be a short one and may be fitted to terminal A or B at will. This will alter the aerial directivity to some extent and if used in conjunction with the aerial tuner shown at Fig. 3 will considerably peak signals using either connection. If the terminals are shorted, a definite drop in signal strength will result.

Providing that bare stranded copper wire is used, the down lead may be tapped on at any point by means of a spring clip (such as in the Windom aerial) one-third from either end, although other points may be tried. If an S meter is available the maximum or peak point can be noted, after which the aerial tuner can be coupled in and a further note taken as to the extra gain obtained.

Insulators



By B. W. Hollinshead

IT is widely accepted that the highest quality of reproduction of radio programmes is obtained by feeding the output of an f.m. tuner into a high fidelity amplifier. The frequency response of these transmissions and their freedom from background noise cannot be matched by even the best a.m. tuners.

However, the disadvantages of the f.m. tuner are its high initial cost, its difficulty to align without proper equipment and the fact that in some areas the v.h.f. service is not readily available.

There must be, however, numerous enthusiasts who would be content with simple equipment, which can be constructed at a comparatively low

cost, to feed their amplifiers and tape recorders and it is to these that the following design is offered.

When considering the design of an a.m. tuner two courses are open. The "superhet" tuner is more complex and presents alignment problems similar in many ways to those of f.m. units. On the credit side it must be said that the superhet has superior selectivity and sensitivity to the t.r.f. or straight set.

However, the t.r.f. tuner unit to be described here will give a higher quality output than a superhet and several of the more powerful Continental stations are within its reach as well as the BBC programmes. Added to this the lack of i.f. transformers etc., will considerably reduce costs. The tuner will be suitable for feeding either an amplifier on tape recorder.

Circuit

Only two valves are used in this circuit, which is shown in Fig. 1. The first valve is a variable-mu r.f. pentode, the type used in the original being an EBF89 with the diodes strapped and earthed. This valve was used simply because the writer had one to hand and there is plenty of latitude for the choice of valve to be used in this position. An EBF80 could be inserted without any change of wiring and for those who have them available a 6BA6 on a B7G base, EF85 or EF89 on B9A bases or even the 6K7 on an octal base might be considered. The only requirement would be that the appropriate cathode bias resistor for the valve should be used instead of the 330\Omega resistor stipulated in the present case.

The detectors uses a double triode ECC82 or 12AU7. The first half of the valve is strapped as a diode, the second half being used as a cathode follower. This arrangement serves two purposes, the diode noted for its low distortion is an excellent detector, while its inherent disadvantage, that of imposing undue clamping on the tuned circuit thus making selectivity rather poor, being overcome by the high impedance of the cathode follower. The cathode follower also allows a fairly long lead to be used for connecting to the amplifier. An ECC81 (12AT7) or ECC83 (12AX7) might be tried

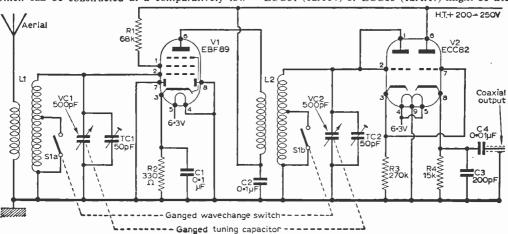


Fig. 1: The circuit.

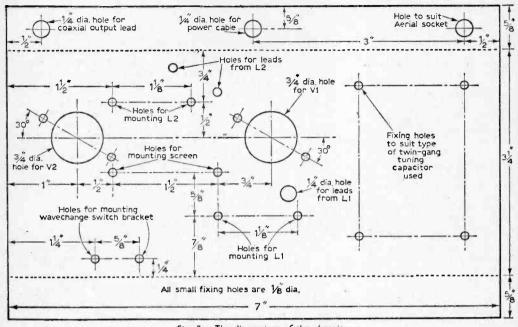


Fig. 2: The dimensions of the chassis.

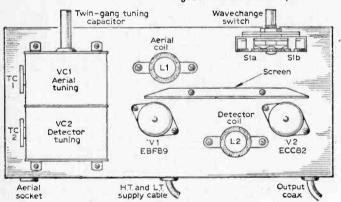


Fig. 3: The above-chassis layout diagram.

in this position if available, having the same base connections. Similarly the octal based 6SN7 or 6SL7 might be tried also.

The R.F. Coils

The coils used in this circuit were Repanco DRM3 dual range t.r.f. coils, the reaction winding being disregarded. These were used for no other reason that the writer had a pair in his spares box, and any similar dual range t.r.f. coils such as the Osmor QA11D or QR11D would suit.

If individual constructors prefer, separate coils could be used for each band but this would add some extra complexity to the switching and cost more. Apart from this the chassis would need to be increased in size to accommodate these extra components. This the writer feels would detract from the designed simplicity of the unit.

The wavechange switch was an ex-Government single-wafer, two-pole, two-way switch obtainable quite cheaply and probably to be found in most spares boxes, or could be easily adapted from a similar switch having more poles

A simple epicyclic reduction drive for the two-gang capacitol makes for easy tuning. The trimmers were chassis mounting compression trimmers taken from an old superhet.

In the writer's tuner the overal

size was kept as small as possible

Construction

without making the chassis un duly cramped. A small tuning capacitor was available and a larger component might require some increase in chassis width. To keep the depth of the chassis to a minimum, both aerial and detector coils were mounted above the chassis, at earthed aluminium screen being fitted as in the drawing (Fig. 3) to prevent any instability. The screen does the job admirably as the tuner is quite

The chassis was cut from a piece of 16s.w.g aluminium sheet measuring 7in. x 4½in. Runner in. deep are marked and bent on the front and rear. Full details are given in Fig. 2. All holes are drilled, those for the valveholders being cut eithe with a chassis punch or by drilling and filing. The valveholders are then fitted with a solder tag unde each bolt after which the tuning capacitor and

stable.

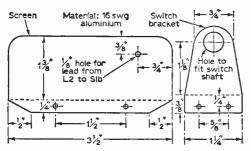


Fig. 4: Details of the screen.

drive are mounted on the right-hand side of the chassis. The method of mounting will vary with different capacitors.

The aluminium screen is drilled after being cut to size according to details given in Fig. 4 and fixed in place with 6B.A. bolts. A bracket is made from aluminium to take the wavechange switch SI and is bent and drilled so that the switch and tuning capacitor shafts are at the same height. This bracket is also held in place with 6B.A. bolts.

The coils are finally bolted in place with the aerial coil at the front of the chassis and the detector coil behind the screen. The trimmers are soldered directly to the tuning capacitor and the earthed ends bolted to the chassis.

Wiring

As most of the components are small they can be wired directly to the valveholder tags. Tinned copper wire is used for connection and covered

COMPONENTS LIST Resistors: 270kΩ 68kΩ R3 RI 330Ω **R4** 15kΩ All 1W, carbon Capacitors: 0·1μF paper 350V 0·1μF paper 350V 200pF silver mica C1 C2 C3 C4 0.01µF paper 350V VC1 500pF VC2 500pF twin-gang tuner 50pF compression type trimmer TCI TC2 50pF compression type trimmer Valves: VI. EBF89 or EBF80 V2 ECC82 Coils: Li, L2 Dual range t.r.f. coils (Repanco DRM3see text) Switch: SI Two pole, two-way rotary **POWER PACK COMPONENTS** 1.8kΩ 1W RI $32\mu F \atop 32\mu F$ dual electrolytic 350V CI C₂ Mains transformer with tapped primary. Secondaries: 0-200V 20mA; 6.3V IA TI Contact cooled rectifier, 250V 20mA

Double-pole, on/off switch

with sleeving where necessary. As some single screened pick-up lead was available the grid lead in the detector circuit was screened although it may not have been absolutely necessary to do so.

The diodes, pins 7 and 8 of the EBF89 were strapped together at the valveholder and earthed together with pin 4 as the heater return. Pins 4 and 5 of the ECC82 are taken to the heater supply via pin 5 of V1. Pin 9 goes to earth. The grid and anode pins of the first half of the ECC82 are strapped to form the diode connections.

The h.t. circuit can then be wired. The anode of the second half of the ECC82 takes its h.t. direct from the h.t. rail without the need for an anode resistor. Similarly the h.t. supply to the anode of V1 via the detector coils does not use a resistor. The feed for the screen grid of V1 is via a 68kΩ resistor R1.

Testing

When all wiring has been completed the tuner

can be connected to a suitable power supply which in the writer's case was taken from the main amplifier. A supply of 200-250V 22mA and 6.3V at 0.6A will be required. Should this not be available from the main amplifier a suitpower able supply circuit is shown in This uses a Fig. 5. contact cooled rectifier and a transformer from a TV converter.

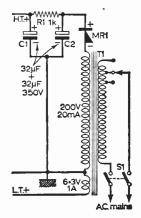


Fig. 5: Circuit of a suitable power-pack.

The output from the tuner is fed via coaxial cable to the amplifier input and a suitable aerial is connected. With the switch in the long waveband position it should be possible to tune the BBC Light Programme at good strength. With the unit switched to medium waves the Home Service is available and, during certain hours, the Third Programme as well. During the evening several Continental stations should be heard. It is only necessary to adjust the trimmers for maximum output and the tuner is completed.

If desired an on/off switch can be fitted to the front of the tuner in the h.t. lead so that the apparatus is always ready for use without waiting for the heaters to warm up.

A pointer was cut from To in. Perspex and fixed to the epicyclic reduction gear with "Araldite" or similar glue. If a front panel is fitted the hole for the drive must be cut and the panel mounted before the pointer is glued in position. The writer's tuner was mounted in a small box with all leads coming from the rear and station names marked on the front panel with transfers.

In conclusion the writer feels that constructors of this tuner will be agreeably surprised both with the performance of this tuner and also with its simplicity and low cost.

A Versatile DOUBLE-TRACE OSCILLOSCOPE By J. H. B. Gould

CONTINUED FROM PAGE 519 OF THE OCTOBER ISSUE

HEN two functions have to be compared by means of an oscilloscope, it is often simplest to do this by using a double trace. Normally, a double-trace display is obtained using a splitbeam or double-gun cathode ray tube; however, practically the same result can be arrived at with a normal tube, using an electronic trace-splitting circuit. The circuit described here uses one valve: a double triode.

Electronic Trace-switching

In order to produce two traces, a single-beam c.r.t. must draw each trace successively. It can do this in three ways:

(1) By completing the one trace and then going on the other, see Fig. 14(a).

(2) By drawing a small section of one trace, then a small section of the other, and continuing until both traces are complete, i.e. "sampling", see Fig. 14(b).

(3) By drawing one trace several times and then carrying out the same process on the other trace.

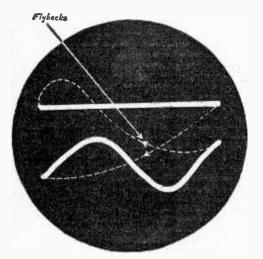


Fig. 14a: Producing two traces from a single-beam c.r.t.: one trace completed, then followed by second trace.

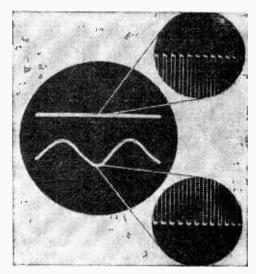


Fig. 14b: Producing two traces from a single-beam c.r.t. "sampling" method.

The circuit can operate in any of these "modes".

As each trace has to carry different information there must be two Y inputs, switched or gated so that they are each applied to the Y deflectors only when the correct trace is being drawn. The existing amplifiers are used for this purpose, controlled by the square-wave output from a multivibrator.

The Trace-switching Circuit

Fig. 16(a) shows a balanced multivibrator, and Fig. 16(b) indicates the waveform it develops. The multivibrator is a two-stage, resistance-coupled amplifier in which the output of the second stage is coupled to the input of the first; the circuit oscillates by virtue of the positive feedback arising out of this coupling. During one half cycle one triode carries a heavy anode current whilst the

-continued on page 61:

OVER

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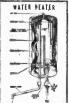
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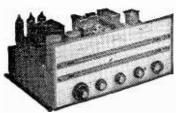
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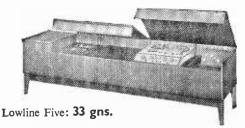
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-continued from page 608

other triode is cut off; then the situation reverses for the other half cycle. This behaviour makes the circuit ideal for controlling the "gating" amplifiers.

As can be seen from Fig. 16(b), each cathode of the multivibrator carries a large positive voltage for half its operating cycle. In practice, (Fig. 17), each cathode returns to earth via the cathode bias resistor of one of the amplifiers "A1" "A2". In this way, one amplifier is always cut off at any given time while the other is operating normally, feeding the trace.

The "Double-beam" position of the Y selector switch

tion of the Y selector switch (S4) connects the outputs of both amplifiers in parallel across the deflector plates, and switches on the multivibrator. It does one other thing: it connects the other Y deflector plate (conventionally known as "Y2") to the slider of a potentiometer (VR10) forming the anode load of one side of the multivibrator (through what has been up till now the Y-plate bypass capacitor); the purpose of this is to separate the two traces.

When the trace-splitting circuit is built into the oscilloscope, the output capacitors of the two amplifiers (C27 of Fig. 12) should be shorted out and removed. If this is not done, the capacitor of the quiescent amplifier will act as a frequency dependent shunt across the plates. The only effect this action will have on normal operation is a movement of the trace when switching from "Plates" to "Amplifiers", and this can easily be corrected using the appropriate shift control.

Once the circuit has been set up, there will normally be little need to touch the intensity-balance control (VR11), so a "preset" type of rheostat is

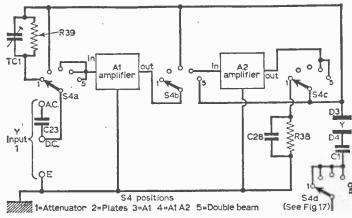


Fig. 15: Selector switching (with beam switching). Otherwise as Fig. 13b.

quite adequate here. However, occasions may arise in which this control could prove useful; for example, where one trace shows a waveform of much greater amplitude than the other. For this reason, it is wirth while mounting this VR11 on a simple aluminium angle-bracket bolted near to the edge of the chassis just clear of the case (to the rear of hole "H" in Fig. 2, for example). Here, it could be operated when necessary by passing the blade of a screwdriver through a matching hole in the outer case.

Operating the Circuit

The two inputs are fed to the X and Y terminals respectively.

Any of the three previously mentioned operating modes can be set up with this circuit. For mode (1), the multivibrator is synchronised at half the timebase frequency; for mode (2) it runs freely at a much higher frequency than that of the timebase (or it can be synchronised at a high multiple of the

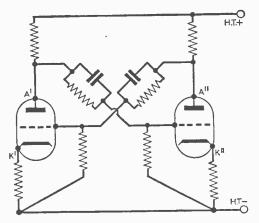
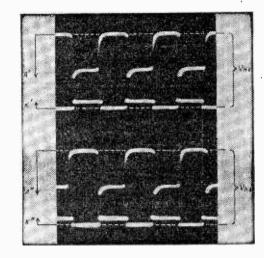


Fig. 16a (above): A balanced multivibrator. Fig. 16b (right): Waveform generated by circuit of Fig. 16a.



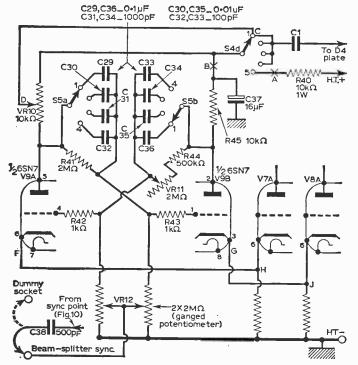


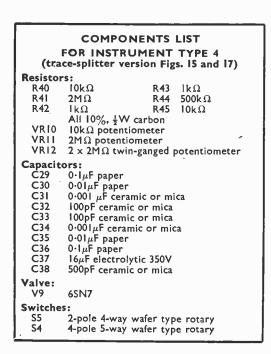
Fig. 17: The trace-splitter circuit, V9a and V9b.

timebase frequency); for mod (3) it is synchronised at a *sub* multiple of the timebase frequency.

The first mode is the onmost commonly employed. The "sampling" mode can find use at very low timebase fre quencies where flicker become a major problem. Mode (3) ha serious disadvantages, but i is useful at very high timebase frequencies, when phase shif in the trace-switching circuisets an upper limit on its usefu operating frequency.

Yet a fourth mode of operation is possible. In this, the two traces are displayed side-by side. To set this up, the multi vibrator is synchronised at the same rate as the timebase and the trace-separation contro turned down to zero. Thi mode can be useful in comparing amplitudes, if the gain set tings of the amplifiers are taker into account.

To avoid damaging the 's selector switch, the instrumen should be switched off before switching to or from the "Double-beam" position.



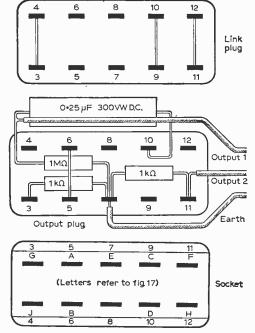


Fig. 18: Link-plug connections for squarewave generator using 10-way Jones plug.

The Controls

There are five controls governing operation of the trace-splitter circuit (see Fig. 17): the Y-selector switch (S4); the trace-splitter frequency switch (S5); the trace-separation potentiometer (VR10); the trace-splitter sync potentiometer (VR12) and the intensity-balance rheostat (VR11).

This last mentioned control has two functions: when the circuit operates in mode (1), it can correct any tendency for one trace to repeat at the expense of the other; in the other two modes it can be used to increase the *brilliunce* of one trace relative to the other. As with the timebase, the sync control should be set at the lowest level at which it is effective.

Using the Circuit as a Square-wave Generator

A square-wave generator is useful for such tasks as checking the frequency response of amplifiers or filter networks. In order to use the trace-splitter circuit as a square-wave generator, a number of circuit changes must be made on each occasion. By far the easiest way of making these changes automatically is to use the link-plug method.

Fig. 19: Trace-splitter sync sockets.

For this, a socket is necessary on the oscilloscope. There is not likely to be much room for this on the panel, and it could just as well be mounted on the chassis near to the multivibrator and facing a hole cut into the outer case. A ten-way Jones type connector is ideal for this job, with the female member mounted on the instrument to prevent shocks should it be handled accidentally.

The circuit of Fig. 17 must be modified by removing the two leads joining the cathodes of the multivibrator to those of the amplifiers and also that joining the slider of the trace-separation potentiometer (VR10) to the Y selector switch (S44). These points are then wired to the link socket as shown in Fig. 18.

During normal operation, a link plug is left in this socket; but when a square-wave output is required this plug is removed and replaced by another plug carrying the output leads.

Warning: About 250V d.c. can exist between pin 10 of the square-wave output plug and one of the leads under certain circumstances after the plug has been removed. This will persist until the charge on the capacitor has leaked away.

In this condition, the frequency and sync controls retain their original functions. However, the trace-separation control now becomes an amplitude control for Output 1 and the intensity-balance control determines the waveform of the outputs, particularly the "mark-space" ratio.

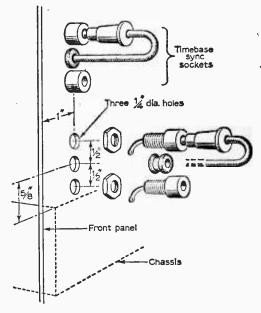
With the output plug in position, the Y selector switch can operate in any position except "Double-beam", which is now out of action.

The sync input is fed from a socket on the front panel so that the trace-splitter circuit can be synchronised from an external source if desired. To save using a switch, the timebase generator synchronising waveform is brought to another socket by a wander plug, which can be transferred to a dummy socket when using external sync.

This plug and socket arrangement is similar to that used for selecting either internal or external sync for the timebase generator. Details of the additional drilling required are given in Fig. 19. It will be seen by referring to Fig. 1 that the trace-splitter sync sockets are located immediately below those for the timebase generator.

Oscillography

Many excellent oscillograph cameras are available for use with cathoderay oscilloscopes. These are not an economic proposition for the amateur,



however, and it is proposed to conclude the present series by describing a simple method of using an ordinary 35mm, still camera.

Only recurrent displays will be dealt with, as transient waveforms demand either a motor-driven camera or an oscilloscope equipped with a single-sweep timebase. But it should be remembered that the term "recurrent display" covers not only waveform on a linear timebase, but any kind of steady pattern: Lissajous figures, valve and transistor characteristics, amplifier input/output characteristics and the like.

The screen of an oscilloscope is a very small target for a normal camera, so to obtain any results worth having, the lens must be brought close to the screen. The first problem, then, is to focus the camera at this short range. The simplest method is to use a "No. 3" or +3 diopter supple-

-continued on page 657

V. E. HOLLEY describes

the conversion of a CAR RADIO for A.C. Mains Operation

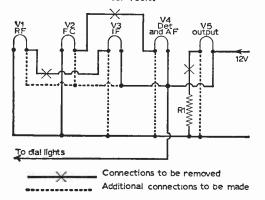
A SIMPLE AND INEXPENSIVE CONVERSION WILL PROVIDE A HIGH QUALITY DOMESTIC RECEIVER

OW that most car radios of current manufacture employ transistors, the older valve type receivers can often be picked up quite cheaply secondhand. These car radio receivers incorporate an r.f. stage and the gain, selectivity and a.g.c. performance are all better than average kind of broadcast receiver. It is only necessary to provide a mains power pack and a reasonable aerial, to produce a domestic receiver which will give a good account of itself and will be especially useful in areas where reception conditions are poor. Conversion is a simple task which may be undertaken with confidence.

Valve Heaters

Virtually the only alteration required in the receiver itself is to the heater wiring. The heaters will almost certainly be wired in series pairs, a series resistor being used on one valve to complete the pairs for 12V operation. The heaters must be paralleled for 6.3V working. The original circuit will look something like Fig. 1 (solid lines) which shows the connections to be removed and the additional ones to be made. The 12V dial lights will, of course, need to be replaced by 6.3V bulbs.

Fig. 1 (below): A typical heater chain circuit of a car radio.



H.T. Requirements

The h.t. requirement will be between 60 and 70mA as a rule, at a voltage somewhere between 200 and 250. The voltage can be determined within close limits by examination of the output stage.

For example, in the prototype conversion, the output valve, an EL42, was found from the valve list to require an anode voltage of 225. Allowing for bias and for voltage drop in the primary of the output transformer, an h.t. voltage of 235 was deduced. The power pack was designed accordingly to the circuit of Fig. 2. Here, a valve rectifier, 6X4, is used in a full wave circuit and the d.c.

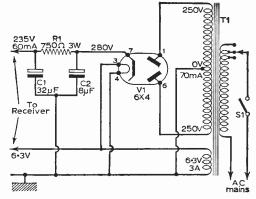


Fig. 21 The circuit of the mains power pack.

voltage available at its cathode is 280 with an $8\mu F$ reservoir capacitor. About 45V must therefore be dropped in the smoothing resistor R1. Reference to valve lists showed that the h.t. consumption of the receiver should be about 60mA, and R1 was therefore given a value of 750Ω , which, in association with the capacitors C1 and C2, provides adequate smoothing.

The transformer used had only a single 6.3V winding. If a separate rectifier winding is available, it is good practice to use it and so avoid having a large difference of potential between the rectifier heater and cathode. The power supplies

can be fed into the receiver through the socket to which the original power pack was connected.

transformer primary. The original wiring to the switch should, of course, be removed.

Construction

It is convenient if the new pack can be built on to the receiver to form a single complete unit, and this was accomplished in the writer's case by constructing the pack on a chassis of 18s.w.g. sheet aluminium, fitted over the rear of the receiver as

shown in the photograph. This chassis provides support for the new components, covers the rear of the receiver which would otherwise be unprotected after removal from its original case, and leaves

A car radio converted by the author to operate from a.c. mains.

a space available above the receiver controls to accommodate a 7in. x 4in. elliptical loudspeaker.

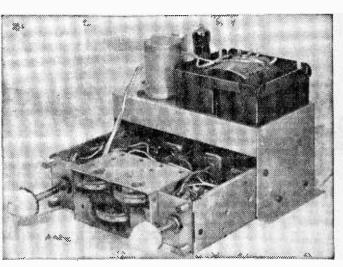
Unless the set to be converted is a very old one, it will conform to the standard car radio measurements of 7in. x 7in. x 2in., and the chassis dimensions given in Fig. 3 will hold good.

The arrangement of the components is entirely a matter of convenience—Fig. 3 gives an idea

of the prototype layout together with details of the wiring. The mains supply should be taken into the receiver chassis close to the on/off switch, passed through the switch and taken thence to the mains

Testing

Before putting the converted receiver into service, the h.t. line voltage should be checked at the anode of the output valve and the value of the smoothing resistor altered if necessary to bring the line voltage to within $\pm 10 \text{V}$ of the correct value. In this connection, it should be noted that some of the older car radios carry a smoothing resistor and



capacitor in the receiver chassis and if these are found to be present, their equivalents, R1 and C1 (Fig. 2), may be omitted from the new power pack.

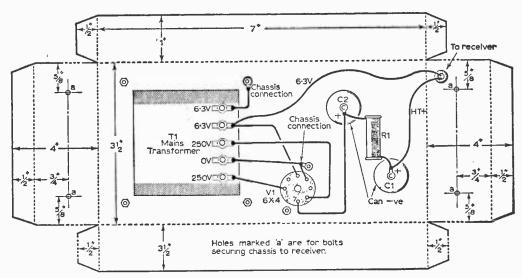


Fig. 3: The wiring diagram and chassis details.

electronic DOOR CHIMES and BURGLAR ALARM

By R. Bebbington

ANY variations are possible on the electronic chimes theme to be described. It is as well therefore to discuss these at the outset so that constructors may weigh up the pros and cons before getting involved in circuit details.

In its entirety the circuit consists of two sections, a high frequency oscillator for the burglar alarm and a low frequency oscillator to produce the chimes. The h.f. oscillator is arranged to be just on the point of oscillation so that any slight variation in the grid capacitance, for example the presence of an intruder, will cause oscillations to cease. This allows the second triode to conduct and to operate a relay in its anode circuit, and the relay contacts supply the chime oscillator with h.t.

Should the constructor already possess door chimes, these can be operated by connecting the relay contacts in place of, or across the existing bell-push. This would, of course, dispense with the circuitry of V2. Alternatively a dummy bell-push could be used consisting of a metal plate connected to V1 grid circuit. As the hand approaches this, the chimes would sound in anticipation, as it were, of the now bewildered caller.

Many other novel uses of this proximity device spring to mind, including displays for bazaars,

etc. The relay contacts may be wired to operate bells, bulbs or more ingenious

devices.

For the constructor who decides that he is burglar-proof or perhaps has nothing worth stealing, the chime circuit alone is well worth constructing. As this constitutes the heart of the circuit we shall now consider it in some detail.

Basic Hartley Chime Oscillator

Designed around the ubiquitous 12AU7 double-triode, this Hartley oscillator is capable of realistic

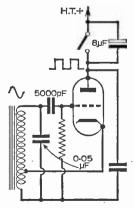


Fig. 1: The basic Hartley oscillator circuit.

chime effects, the basic circuit being shown in Fig. 1 The frequency determining components are the centre-tapped coil and the $0.05\mu F$ capacitor across it. The formula for calculating the required values of these components for a given frequency is the

well known $f = \frac{1}{2\pi\sqrt{LC}}$. This is less formidable it both sides are squared, and values of L and C car

then be easily found by interpolation.

For example: $f^2 = \frac{1}{4\pi^2 LC}$ therefore $L = \frac{1}{4\pi^2 f^2 C}$

 $4\pi^2$ f²C It will be noted that this is only calculated approximately, as component tolerances and the self-capacitance of the choke would need to be taken into account for accurate calculation.

Coupling to the valve is via the $0.005\mu F$ capacitor and is so small that valve characteristics and h.t supplies have little or no effect on frequency. This important feature is exploited in the method employed to give the notes their chime-like sound. These are characterised by a rapid initiation of the note and a sustained decay time; the $8\mu F$ capacitor in the anode circuit gives rise to the latter effect. On release of the push-button the capacitor tends to charge through the valve and maintains oscillations for a period depending upon the value of this capacitor. As the frequency is substantially independent of the h.t. supply the note remains at the same pitch as it decays. The $8\mu F$ gives a decay time of about 1sec.

It will be realised from the foregoing that this circuit could usefully be employed in electronic organ circuits with the sustain capacitor switched in for special effects.

Practical Chime Circuit

For those interested primarily in the chime oscillator a practical circuit is shown in Fig. 2.

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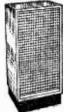
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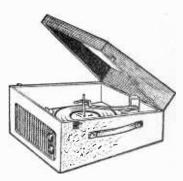
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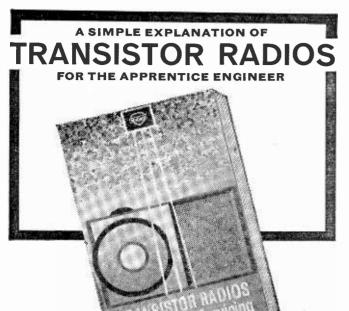
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(Block letters)

This combines the basic circuit of Fig. 1 with an amplifying stage to provide the necessary power to

supply the loudspeaker.

The push-button S1 used in the original version was an ex-government type, and one set of contacts was arranged to make before the other. This means that the h.t. supply makes momentarily before the auxiliary capacitor is switched across the tuned circuit. On depressing the button the oscillator sounds the note determined by the 0.05 µF capacitor C2. As the second contact brings the auxiliary capacitor C1 in parallel, a lower note sounds; when this contact releases the original

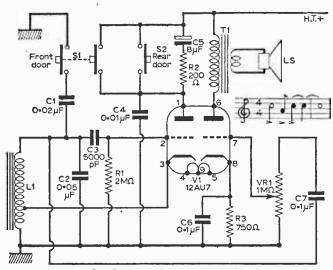


Fig. 2: A practical chime circuit.

COMPONENTS LIST ELECTRONIC DOOR CHIMES (FIG. 2)

Resistors:

RI $2M\Omega$ R3 750Ω

R₂ 200Ω

Ali ½W carbon

VRI IM $\tilde{\Omega}$ carbon potentiometer

Capacitors: Cl 0.02μ

0.02µF paper

C2 C3 0.05µF paper

5000pF ceramic or mica

C4 0.01 µF paper

8μF electrolytic 250V

 $0 \cdot I \mu F$ paper $0 \cdot I \mu F$ paper

Miscellaneous:

SI Push-button switch d.p.s.t. (see text). LI

Tapped coil 200mH approx., iron core (Repanco AF2).

Standard output transformer (Repanco TI

MOTI).

VΤ 12AU7 or ECC82.

3000 type relay, 2 make contacts and 1 RL break contact.

note is repeated and is sustained for a second or so by the current stored in the electrolytic capacitor C5. Thus three notes are chimed in quick succession, the first and third being of the same pitch.

By suitable choice of capacitor values these notes can be arranged to be of any musical pitch. The three sounded by the values specification in Fig. 2 given were C' (524c/s), A (440c/s), followed by C' (524c/s). Appropriately enough, this musical figure is reminiscent of the word "I'm Coming" figure is reminiscent of the word "I'm Coming" in the well-known negro spiritual "Poor Old Joe".

An extra push-button S2 is shown connected

across the h.t. switch and serves admirably for another door. In this case only the upper note would sound to distinguish it from the first push-button which could be located at the front door.

It will be noticed that the coupling to the output stage is taken from the grid circuit. This is preferable because of the smoother waveform obtainable directly from the tuned circuit than if taken off the anode circuit. There is more than sufficient output to load fully the second stage, and the 1M variable VR1 controls the signal fed to the second grid. The output stage is conventional and any standard output transformer and loudspeaker may be used.

Combined Chime and Alarm Circuit

The circuit for a combined chime and alarm unit is given in Fig. 3. It will be noted that the

chimes section is almost identical to the one described above, with the exception that it is controlled by a relay in the alarm circuit instead of by

the push-button of Fig. 2.

The first half of V1 constitutes a high frequency oscillator, the frequency being determined by L1 and C2. Here again the frequency is not critical and the coil used had an iron dust core to enable it to be tuned clear of the Light Programme. The grid coupling capacitor VC1 consists of an airspaced trimmer and this is adjusted so that the tuned circuit is just oscillating. Part of this waveform is rectified by the germanium diode D1 and the resulting d.c. potential employed to bias off the second half of the valve. This bias condition can be critically set by means of the potentiometer VR1.

A metal plate or a strip of foil may be used as the sensing element, the change in capacitance of which stops oscillations and removes this bias.

When the bias is removed the second half of VI conducts and the relay RL is energised through its own contact RL1. At the same time C2 charges and delays the release of the relay which occurs hecause contacts are now open. On release, contacts again make and provide an energising circuit once more and a cyclic operation of the relay ensues. This persists until oscillations are

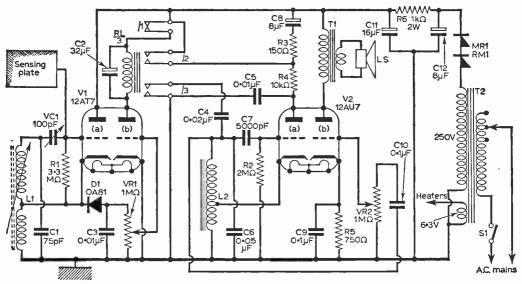


Fig. 3: The circuit of the combined door chimes and burglar alarm.

restored by the removal of the additional capacity, i.e. the intruder.

The other relay contacts switch the chime circuit. Contact /2 provides h.t. and /3 alters the pitch by placing an auxiliary tuning capacitor C4 across the coil L2. As the relay energises, this capacitor will cause the lower note to sound, whilst on release the upper note will ring out due to the sustaining action of C8, and the fact that C4 is not now in circuit.

Power Supplies

The valve heaters may be fed from either a 6.3V or 12.6V winding as convenient. Pins 4 and 5 should be connected to a 12V winding, but if a 6V supply is used pins 4 and 5 should be strapped to one side of the winding and pin 9 used for the other side. The remainder of the power pack calls for little comment, two RM1 rectifiers being used in an orthodox half-wave circuit.

Construction

Very few restrictions are necessary in the methods of construction and layout with regards to the circuits described. Suffice to say that the grid leads for VI should be kept reasonably short to keep stray capacitances to a minimum. The 100µF variable trimmer VC1 should also be mounted clear of the chassis as neither side goes directly to earth. The chime oscillator section is by no means temperamental and consequently does not dictate any set disposition of components. So plug in that soldering iron and "sound out" these novel circuits!

COMPONENTS LIST

COMBINED CHIMES AND BURGLAR ALARM (FIG. 3)

Resistors:

RΙ 3-3MΩ I0kΩ R4 R2 $2M\Omega$ R5 750Ω R3 150Ω lkΩ2W R6

All ½W carbon unless otherwise stated

VRI IM Ω carbon potentiometer

VR2 IM Ω carbon potentiometer

Capacitors: Cl 75pF

75pF mica or ceramic

Č2 32μF electrolytic 250V

0.01μF paper 0.02μF paper 0.01μF paper 0.05μF paper C3

C4

C5 C6

C7 5000pF ceramic or mica

C8 C9 8μF electrolytic 250V

0·IμF paper 0·IμF paper

CIO

CII 16µF electrolytic 250V

C12 8µF electrolytic 350V

VCI 100pF air spaced trimmer

Miscellaneous

LI L.W. coil with iron dust core (Repanco RAI).

L2 Tapped coil 200mH approx., iron core (Repanco AF2).

ON/OFF switch

TI Standard output transformer (Repanco MOTI).

T2 Mains transformer, secondaries: 60mA; 6.3V 0.6A or 12.6V 0.3A.

V١ 12AT7 or ECC81.

V2 12AU7 or ECC82.

Rectifiers:

DI OA81 Germanium diode.

MRI Metal rectifier. 2 x RM7 (125V 60 mA).

Showtime Round-up

A summary of the new models seen at the recent series of trade exhibitions. The tables show brand new models only and do not represent the complete range of the manufacturers concerned. See the November Practical Television for details of the new TV sets.

TRANSISTOR PORTABLE RADIOS

It was difficult to detect any startling external changes in the wide ranges of transistor radios to be seen, but the tiny "personal" receivers seem to be on the decline and the trend is towards larger receivers with better sound quality.

The number of transistor sets giving short-wave coverage and facilities for receiving the v.h.f.-f.m. programmes is slowly increasing, but even so in these, and almost all other varieties, prices remain keenly competitive and many sets seen represent extremely high value for money. Readers will also note in the details below the appearance of several extremely advanced transistor sets in the

higher price bracket.

Some "features" of several years ago are virtually standard fittings nowadays—such things as car aerial sockets and tape recorder sockets. From the presentation point of view more models are appearing with solid wooden cabinets.

THE RADIOGRAM

One of the most obvious impressions gained from the tour of exhibitions was that the radio-gram is back with a bang! For some time the radiogram, once almost abandoned, has been

TRANS	ISTOR PORTABLE RAD	OIOS	
Model	Wavebands	Price	Notes
ALBA III Starling	LW, MW	II gns.	3" speaker. Carrying case.
777 Swan	LW, MW	II½ gns.	Wood case, press buttons.
COSSOR CRISIOT	LW, MW	13 gns.	Wood cabinet. Push buttons
DANSETTE Herald	LW, MW	15 gns.	Wood case.
Stanmore	LW, MW	16 gns.	Wood case.
Imp	LW, MW	ll gns.	Measures $8 \times 3\frac{1}{2} \times 1\frac{1}{2}$.
International	LW, MW, SW	19 gns.	
EKCO PT426 Valentine	LW, MW	16 gns.	8 semiconductors.
PBT425 Varsity	LW, MW	19 gns.	8-transistor mains/battery
PT424 New Verity	LW, MW, VHF	22 gns.	receiver. 9 transistors.
FIDELITY Fairline	LW, MW, SW	17 gns.	12 transistors, meter-type
FIDELIT FAITING		17 giis.	tuning indicator, battery level indicator, dial illumination, etc.
GRUNDIG 99 Transonette	LW, MW, SW, VHF	45 gns.	9 transistors, IW to 6 x 4" speaker.
203 Export Boy	SW1, SW2, SW3, MW	37 gns.	9 transistors, IW to 6 x 4" speaker.
Automatic Boy	LW, MW, SW, VHF	£63	internal batteries or 6/12\ car supply, AFC on f.m., T and B tone controls, 2W to 7 x 5" speaker.
TR17	LW, MW, SWI, SW2, SW3, VHF	77 gns.	Two speakers, AFC on f.m. B and T controls, 1.5W out put, sockets for ext. aerial, car aerial, pickup, tape re corder, phones and speaker
KOLSTER-BRANDES WP21 New Lyric	LW, MW	13 gns.	Will amplify incoming 'phone calls and can be used as a baby alarm.
PAM 5215	LW, MW	12½ gns.	as a subject to
5217	LW, MW	17 gns.	Push buttons.
5219	LW, MW	19 gns.	0 semiconductors.
PERDIO Mini-77	LW, MW	10 gns.	With leather carrying case.
Strand de luxe	LW, MW	12 gns.	With leather carrying case.
PHILIPS 214T	LW, MW	13 gns.	4" speaker. Wood cabinet.
REGENTONE BT22	LW. MW	15 gns.	Measures II x 3 x 63".
BT23	LW, MW	9½ gns.	Measures $8\frac{1}{2} \times 2\frac{1}{4} \times 5^{"}$.
R.G.D. B62	LW, MW	15 gns.	400mVV to 4" speaker.
STELLA ST430T	LW, MW, VHF	23 gns.	Separate a.m. and f.m. tunin
ULTRA 6114	LW, MW, VHF	15½ gns.	

Model		RADIOGRAMS	-		
Model ACE Continental Wavebands LW, MW, VHF Mono As gens. LW, Mono As gens. LW, MW, VHF Notes Bass and treble controls. 6V. 10 x 4½* speakers. Stereo Speaker. Nordic LW, MW, VHF Stereo Stereo Speaker. Stereo Speaker. Band T controls. 6V. 10 x 4½* speakers. Stereo Speaker. Stereo Speaker. Band T controls. 6V. 10 x 4½* speakers. Stereo Speaker. Stereo Speaker. Band T controls. 6V. 10 x 4½* speakers. Stereo Speaker. Stereo Speaker. Band T controls. 6V. 10 x 4½* speakers. Stereo Speaker. Stereo Speaker. Band T controls. 6V. 10 x 4½* speakers. Stereo Speaker. Stereo Speaker. Stereo Speaker. Stereo Speaker. Stereo Speaker. Stereo As Speakers. SW per channel. In Speakers. SW per channel. In Speakers. SW per channel. Stereo Speakers. SW per channel. Sw Speakers. SW per channel. Sw Speakers. S		MADIOGIANIS	Steren n		
ACE Continental LW, MW, VHF Stereo Nordic LW, MW, VHF Stereo Nordic LW, MW, VHF Stereo Stereo Stereo Stereo TBA ACE Continental LW, MW, VHF Stereo ACI 31 Imperial RC 133 Imperial LW, MW, VHF STEREO ACI 31 Imperial LW, MW, VHF STEREO ACI 32 Imperial LW, MW, SW, VHF STEREO ACI 32 Imperial LW, MW, SW, VHF STEREO ACI 32 Imperial LW, MW, SW, VHF STEREO ACI 35 Imperial LW, MW, SW, VHF STEREO ACI 32 Imperial LW, MW, SW, VHF ACI 32 Imperial L	Model	Wavehands			Notes
Slimline					
Nordic		,,			
Nordic					
Nordic	Slimline	LW, MW, VHF	Stereo	59 gns.	B and T controls, 5W
COSSOR CRI504A LW, MW, VHF Stereo DANSETTE RG250 Sonata RG133 Imperial RGS144 Concerto LW, MW, W, VHF ELIZABETHAN RG1 LW, MW, VHF Stereo LW, MW, SW, VHF Stereo RG130 Imperial RGS144 Concerto LW, MW, SW, VHF Stereo RG130 Imperial RGS144 Concerto LW, MW, SW, VHF Stereo RG130 Imperial RGS144 Concerto LW, MW, SW, VHF Stereo RG13 Imperial RG5144 Concerto LW, MW, SW, VHF Stereo RG10 RM, SW, W, W					
COSSOR CRI504A	Nordic	LW, MW, SW, VHF	Stereo	89 gns.	
COSSOR CRI504A LW, MW, VHF Stereo TBA 3W per channel via 8 x 5 speakers. 8 x 5' speakers. 8 x 5' speakers. 8 x 5' speakers. 8 x 5' speakers. 110 gns. Stereo 5 tereo 5 tereo 6 7 gns. 110 gns. Stereo 67 gns. 110 x 6' speakers. FM multiplex output. Model 600 is an a.monly version at 51 gns. Model 600 is an a.monly version at 51 gns. Model 50A is an a.monly version at 51 gns. Model 600 is an a.monly version at 51 gns. Model 50A is an a.monly version at 51 gns. Model 50A is an a.monly version at 39 gns. 8 x 5' speaker. FM multiplex output. Model 600 is an a.monly version at 39 gns. 8 x 5' speaker. FM multiplex output. Model 600 is an a.monly version at 39 gns. Model 50A is an a.monly version at 39 gns. 8 x 5' speaker. The feather for multiplex output. Model 600 is an a.monly version at 39 gns. 8 x 5' speaker. The feather for multiplex output. Model 600 is an a.monly version at 39 gns. 8 x 5' speaker. The feather for multiplex output. Model 600 is an a.monly version at 39 gns. 8 x 5' speaker. The feather for multiplex output version at 39 gns. 8 x 5' speaker. The feather for multiplex output version for reverb. As above. Stereo 19 gns. Stereo 66 gns. Stereo 7 gns. Stereo 7 gns. Stereo 7 gns. Stereo 7 gns. Stereo 8 gns. Stereo 19 gns. Ster			•		
None	COSSOR CRISO4A	IW MW VHE	Storeo	TRA	
DANSETTE RG250 Sonata RG133 Imperial LW, MW, WHF RG131 IW, MW, WHF RG14 IW, MW, SW, VHF Stereo Stereo Stereo Filo grs. Stereo 8 x 5' speakers. Speakers. Stereo Filo grs. Filo grs	COSSOR CRISTIA	_ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	366,60	IDA	8 x 5 speakers.
RGSI44 Concerto ELIZABETHAN RG1 LW, MW, SW, VHF Stereo FALCON Manhattan 800 LW, MW, SW, VHF Stereo Tudor 60FM Mono Tudor 60FM LW, MW, SW, VHF Tudor 60FM Mono Tudor 60FM Model 50A an Model 50A s. an Model 50A s. an Model	DANSETTE RG250 Sonata	LW, MW, VHF	Mono	59 gns.	
RGSI44 Concerto ELIZABETHAN RG1 LW, MW, SW, VHF Stereo FALCON Manhattan 800 LW, MW, SW, VHF Stereo Tudor 60FM Mono Tudor 60FM LW, MW, SW, VHF Tudor 60FM Mono Tudor 60FM Model 50A an Model 50A s. an Model 50A s. an Model		LW, MW, VHF	Stereo		8 × 5" speakers.
FALCON Manhattan 800 LW, MW, SW, VHF Mono Stereo Sp gns. Model 600 is an a.monly version at 51 gns. Model 50A is an a.m. version (LW, MW, SW) and Sy gns. LW, MW, SW, VHF Carmel F24 LW, MW, SW, VHF Carmel F24 LW, MW, SW, VHF Stereo GRUNDIG MS20 Hilton LW, MW, SW, VHF Stereo MS10 KS80 Baroque LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF MS100 Kingsley LW, M		LW, MW, SW, VHF			
Tudor 60FM	ELIZABETHAN RGI	LW, MW, VHF	Stereo	67 gns.	
Tudor 60FM LW, MW, VHF Mono 35 gns. Model 50A is an a.m. version (LW, MW, SW) at 32 gns. Consort Carmel F24 LW, MW, SW, VHF Carmel F24	FALCON Manhaura 900	LVA/ MVA/ CVA/ V/LIE	Ceans-	EQ	
Tudor 60FM LW, MW, VHF Mono S gns. Model 50A is an a.m. version (LW, MW, SW) at 32 gns. C Consort C Carmel F24 LW, MW, SW, VHF C Carmel F24 LW, MW, SW, VHF Stereo GRUNDIG MS20 Hilton LW, MW, SW, VHF KS80 Baroque LW, MW, SW, VHF KS80 Bar	PALCON Mannattan 800	LVV, 11VV, 3VV, VIII	stereo	37 giis.	
Version (LW, MW, SW) at 32 gns.	Tudor 60FM	LW. MW. VHE	Mono	35 gns.	
Consort Carmel F24		,,			
Consort Carmel F24 LW, MW, SW, VHF Stereo Carmel F24 LW, MW, SW, VHF Stereo Carmel F24 LW, MW, SW, VHF Stereo CARMENT STERED STEREO GRUNDIG MS20 Hilton LW, MW, SW, VHF Stereo CARMENT STEREO CABINET STEREO CABINE					SW) at 32 gns.
G.E.C. G985 GRUNDIG MS20 Hilton MS10 KS80 Baroque LW, MW, SW, VHF LW, MW, SW, VHF Stereo KS80 Baroque LW, MW, SW, VHF Stereo KS80 Baroque LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF MS100 Kings					
G.E.C. G985 GRUNDIG MS20 Hilton MS10 KS80 Baroque LW, MW, SW, VHF KS80 Baroque LW, MW, SW, VHF Eleve MS100 Kingsley LW, MW, SW, VHF Mono Eleve Eleve Mono Eleve Mono Eleve Eleve Eleve Eleve Eleve Mono Eleve El	Carmel F24	LW, MW, SW, VHF	Stereo	45 gns.	
GRUNDIG MS20 Hilton LW, MW, SW, VHF Stereo 119 gns. Decoder for multiplex. Provision for reverb. MS10 LW, MW, SW, VHF Stereo 370 gns. As above. KS80 Baroque LW, MW, SW, VHF Stereo 370 gns. Switchable AFC, 3 tone controls, multiplex decoder, reverb., etc. MS100 Kingsley LW, MW, SW, VHF Stereo 395 gns. 15W per channel, 6 speakers, multiplex decoder, reverb. unit. PH3030 LW, MW, SW, VHF Stereo 66 gns. 3W via 8½ x 4½" speakers. Table gram. KOLSTER-BRANDES WG15 Polonaise LW, MW, SW, VHF Stereo TBA 3W output via 8 x 5" speakers. MURPHY A881SR LW, MW, VHF Stereo 85 gns. 3W output via 8 x 5" speakers. PAM 5212 LW, MW, VHF Mono 5tereo 57½ gns. PHILIPS 420 LW, MW, VHF Mono 56 gns. LW, MW, SW, VHF Stereo 56 gns. LW, MW, SW, VHF Stereo 11 valves.	G E G C005	1347 54347	M	TDA	
MS10 KS80 Baroque LW, MW, SW, VHF Stereo KS80 Baroque LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF Mono LW, MW, SW, VHF Stereo MASTERADIO D573 LW, MW, SW, VHF Stereo MASTERADIO D573 LW, MW, SW, VHF Stereo MASTERADIO D573 MURPHY A881SR LW, MW, VHF Stereo LW, MW, VHF Stereo MASTERADIO D573 MURPHY A881SR LW, MW, VHF Mono Stereo MASTERADIO D573 MURPHY A881SR LW, MW, VHF MOno Stereo MASTERADIO D573 LW, MW, VHF MOno Stereo MOno Stereo Mono Stereo Mono Stereo Mono Stereo S7½ gns. S6 gns. S6 gns. S12 gns. SW vickable AFC, 3 tone controls, Multiplex decoder, reverb. Speakers, multiplex decoder, reverb. Speakers, multiplex decoder, reverb. Switchable AFC, 3 tone controls, Multiplex decoder, reverb. Seeakers, multiplex decoder, reverb. Switchable AFC, 3 tone controls, Switchable Speakers, Multiplex decoder, reverb. Switchable AFC, 3 tone controls, Switchable Speakers, Multiplex decoder, reverb. Switchable Speakers, Multiplex decoder, reverb. Switchable Speakers, Multi					
MS10 KS80 Baroque LW, MW, SW, VHF Stereo Stereo MS100 Kingsley LW, MW, SW, VHF Mono Cagns. Stereo MASTERADIO D573 LW, MW, SW, VHF Stereo MASTERADIO D573 LW, MW, SW, VHF Stereo MW, VHF Stereo MW, SW, VHF Stereo MW, SW, VHF Stereo MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF Stereo Mono MS100 Kingsley MONO MS100 Kingsley MS20 kingsley M	GROTADIG 11320 Hillon	L V V, 11 V V, 3 V V, V I II	3(6) 60	117 giis.	
KS80 Baroque LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF Stereo MS100 Kingsley LW, MW, SW, VHF PH3030 LW, MW, SW, VHF Mono Controls, multiplex decoder, reverb., etc. 15W per channel, 6 speakers, multiplex decoder, reverb. unit. Stereo MOLSTER-BRANDES WG15 Polonaise MASTERADIO D573 MURPHY A881SR LW, MW, SW, VHF Stereo MW, WW, VHF Stereo Stereo Stereo MONO Stereo MONO Stereo MONO M	MSIO	LW, MW, SW, VHF	Stereo	93 gns.	
MS100 Kingsley LW, MW, SW, VHF Stereo PH3030 LW, MW, SW, VHF Mono 62 gns. 395 gns. KOLSTER-BRANDES WG15 Polonaise MASTERADIO D573 LW, MW, SW, VHF LW, MW, SW, VHF Stereo MURPHY A881SR LW, MW, VHF Stereo B5 gns. TBA Woutput via 8 x 5" speakers. TBA Woutput via 8 x 5" speakers. TBA Woutput via 8 x 5" speakers. TV valves and 12 semiconductors. 10 x 6" and 4" speakers in each channel. LW, MW, VHF Stereo PAM 5212 LW, MW, VHF Stereo S17½ gns. F129 gns. LW, MW, VHF Stereo S6 gns. LW, MW, VHF S129 LW, MW, VHF S120 LW, MW, WHF	KS80 Baroque				Switchable AFC, 3 tone
MS100 Kingsley					
## Speakers in unitiplex decoder, reverb. unit. ### Word of 2 gns. ### Word of 3 gns. ### Word of 2 gns. ### Word of 2 gns. ### Word of 2 gns. ### Word of 3 gns	MC100 K: 1		•	205	
PH3030	MS100 Kingsley	LW, MW, SW, VHF	Stereo	395 gns.	
PH3030					
KOLSTER-BRANDES WG15 Polonaise LW, MW, SW, VHF Stereo MASTERADIO D573	PH3030	LW. MW. SW. VHF	Mono	62 gns.	
MASTERADIO D573 LW, MW, VHF Stereo TBÅ 3W output via 8 x 5" speakers. MURPHY A88ISR LW, MW, VHF Stereo 85 gns. 7 valves and 12 semiconductors. 10 x 6" and 4" speakers in each channel. PAM 5212 LW, MW, VHF Mono 42 gns. 57½ gns. 57½ gns. Cabinet only 8¼" deep. PHILIPS 420 LW, MW, VHF Mono 56 gns. 56 gns. 11 valves. 526 LW, MW, SW, VHF Stereo 129 gns. 11 valves.				٠	speaker. Table gram.
## Stereo ## Ste					
MURPHY A881SR LW, MW, VHF Stereo 85 gns. 7 valves and 12 semiconductors. 10 x 6" and 4" speakers in each channel. PAM 5212 LW, MW, VHF Mono 5210 42 gns. 5210 Cabinet only 8¼" deep. PHILIPS 420 LW, MW, VHF Mono 56 gns. LW, MW, SW, VHF Stereo 129 gns. 11 valves.	MASTERADIO D573	LW, MW, VHF	Stereo	TBA	
semiconductors. PAM 5212 LW, MW, VHF Mono 42 gns. Cabinet only $8\frac{1}{4}$ " deep. 5210 LW, MW, VHF Stereo $57\frac{1}{2}$ gns. Cabinet only $8\frac{1}{4}$ " deep. PHILIPS 420 LW, MW, VHF Mono 56 gns. 56 gns. 129 gns. 11 valves.	MILIBRILY ACCIED	1 M/ M/M/ V/HE	Seamon	95 ana	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	MORPHI A0013K	LVV, ITVV, VIII	Stereo	92 KII2*	
PAM 5212 LW, MW, VHF Mono 5210 42 gns. 57½ gns. 57½ gns. 57½ gns. 626 Cabinet only 8¼ deep. 57½ gns. 56 gns. 56 gns. 129 gns. 11 valves.					
5210 LW, MW, VHF Stereo 57½ gns. PHILIPS 420 LW, MW, VHF Mono 56 gns. 526 LW, MW, SW, VHF Stereo 129 gns. 11 valves.					
5210 LW, MW, VHF Stereo 57½ gns. PHILIPS 420 LW, MW, VHF Mono 56 gns. 526 LW, MW, SW, VHF Stereo 129 gns. 11 valves.				42 gns.	Cabinet only 84" deep.
526 LW, MW, SW, VHF Stereo 129 gns. 11 valves.				57½ gns.	'
530 LW, MW, VHF Stereo 77 gns. Two 8" dual-cone		LW, MW, VHF		56 gns.	II andreas
LVV. FIVV. VIII SEEFEO // EIIS. I WO O GUAI-COILE		LVV, MVV, 5VV, VHF			
speakers.	330	LVV, MVV, VIII	stereo	// giis.	
REGENTONE ARG22 LW, MW, SW Mono 37½ gns. Cabinet only	REGENTONE ARG22	LW, MW, SW	Mono	37½ gns.	
$29 \times 14 \times 29\frac{1}{2}$ ".				20	$29 \times 14 \times 29\frac{1}{2}$ ".
SRG23 LW, MW, VHF Stereo 55 gns.					
R.G.D. 209 LW, MW, SW, VHF Stereo 75 gns.					
210 LW, MW, VHF Mono 55 gns. SOBELL SG674 LW, MW Mono TBA 8 x 5" speaker.					8 v 5" speaker
STELLA 319A LW, MW, VHF Mono 56 gns. 8" dual-cone speaker.					
325A LW, MW, VHF Stereo 67 gns. 8 x 5" speakers.					
326A LW, MW, VHF Stereo 86 gns. 8" dual-cone speakers.	326A	LW, MW, VHF			
ULTRA 3606 LW, MW, VHF Mono 45 gns.					,
3608 LW, MW, SW, VHF Stereo 59 gns.	3608	LW, MW, SW, VHF	Stereo	59 gns.	

making a come-back. But this year there are more new radiograms than any other type of product. Even companies normally confining themselves to smaller items are now producing radiograms.

The accent was on the "long, low look" type of housing, which has obviously been influenced by

the need for wide cabinets in the stereo models. And here it might be mentioned that in all stereo equipment the separate speaker unit idea is fast going out. No doubt manufacturers have discovered that the lady of the house, who often decides ultimately what to buy, dislikes the

Po	ORTAB	LE RECO	RD PL	AYERS	
Model		er unit		Price	Notes
DANSETTE Monarch	,	UAI5		24 gns.	3½W output via twin 8" speakers, B and T controls, adaptable to stereo.
ELIZABETHAN Pop-20	Gar	rard Auto	slim	27 gns.	Two 8 x 5" speakers in parallel, B and T controls, Tape and Mic. sockets, speakers detachable from unique styled cabinet.
KOLSTER-BRANDES WRPI0 Popet RRP20 Rhythm MASTERADIO D576 D577	BSR BSR			15 gns. 19½ gns. TBA TBA	2W output via 7 × 4" speaker. 7W push-pull via 8 × 5" speaker. High and low level tape outputs, straight-through amplifier
McMICHAEL MI77	BSR	UAI5		ТВА	facilities. 7W push-pull via 8 x 5" speaker. Straight-through amplifier facilities, tape sockets, T and B controls.
PAM 5200 PHILIPS AG4126 REGENTONE AHG33 AHG44 HG15)S	16 gns. 15 gns. 14½ gns. 16½ gns. 9 gns.	$7 \times 4''$ speaker. Operates from six 1.5V batteries. $4\frac{1}{2}''$ speaker. $8 \times 5''$ speaker. B and T controls. 5'' speaker.
R.G.D. 165 SILVERTONE API8	BSR BSR	UA15		17 gns. 28 gns.	8 x 5" speaker, B and T controls. 6W push-pull output to 8 x 5" speaker, B and T controls, adaptable to stereo.
	TAF	E RECO	RDERS	_	
Model	Dęck	Tracks	Speed	ls Price	Features
COSSOR CR1621	Own	2	17	26 gns	Provision for mains unit.
	BS R BSR	4	17, 33 33, 7	$\frac{1}{2}$, $7\frac{1}{2}$ 33 gns. $\frac{1}{2}$ 27 gns.	Many. 3.5W to 7 x 4" speaker, monitor, ext. amp. facilities, etc.
FIDELITY Playmaster	BSR	2	33	20 gns.	
GRUNDIG TK6	Own	2	3 3 , 1	₹ 65 gns.	Level meter, monitor, battery operated (transistorised), battery level indicator.
LEE PRODUCTS 802 Shaftesbury 804 Shaftesbury		2 4	3 ³ / ₄ , 1	26 gns. 33 gns.	Output 3W. Digital counter, monitor facilities.
MASTERADIO D502 PHILIPS EL3586	BSR Own	2 2	334 178	TBA 25 gns.	2.5W to 7 x 3½" speaker. Battery operated with provision for mains unit. 500mW to 4" speaker.
STELLA ST471	Own	2	17	26 gns.	

untidiness caused by having odd pieces of equipment external to the main unit. There was also a noticeable trend towards the more compact type of cabinet, representing a return to a style that lost favour in recent years.

Most of the new radiograms have f.m. facilities, though there were a few a.m.-only models. Most are for stereo record reproduction but a few mono-

only radiograms make their debut.

The prospect of a decision on Multiplex stereo radio broadcasting has prompted several thoughtful manufacturers to produce models wired up for the easy fitting of a decoder unit whenever stereo broadcasting becomes a regular service.

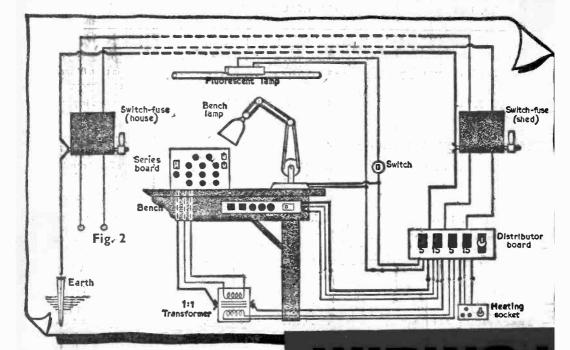
PORTABLE RECORD PLAYERS

These continue to play an important part in the manufacturers' catalogues and a number of new, attractive models were shown for the first time. Most of them are mono, though some are wired for stereo conversion if required. Some have added facilities such as straight play-through. One breaks new ground from the design point of view.

TAPE RECORDERS

The tape recorders on show were not entirely typical of the complete range of products available

-continued on page 657



OW that the increased constructional activity of the winter months is approaching, the radio- and television enthusiast will be checking over his would-be den, remembering the fine plans-for conversion that were formulated in his mind during the summer. At this stage, those plans seem a little ambitious. Converting the potting shed to a workshop has a number of unforeseen snags. The following notes are an attempt to discuss as many of those snags as can be uncovered, and to offer a few solutions.

Supply Regulations

First consideration is the power supply. To comply with the regulations, it must be a

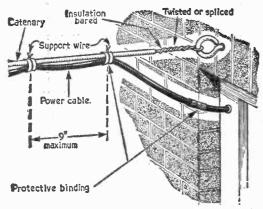


Fig. 1: Using a catenary to carry the power line to the workshop.

separate circuit, completely isolated, fused and switched. This means a switch-fuse at the meter board, a correctly installed run of cable adequate for the proposed load, and a switch-fuse with outlets at the other end. And the local Electricity Board will not connect your switch-fuse to the incoming power line until they are satisfied it complies with both the I.E.E. Regulations and any local interpretations of these.

If one is tempted to by-pass these restrictions, and save time and trouble by plugging the house end of the feed cable into a convenient power point, it should be remembered that in the case of any accident—fire or personal hazard—no insurance company would consider a claim on an uncertified installation.

Perhaps it would be as well for us to know, at the outset, which of the I.E.E. Regulations apply to our conversion of the potting shed. The figures in brackets are those regulations which cover our circumstances, and which will be referred to as we go along. For a more detailed exposition, see I.E.E. Regulations, 13th Edition, 1955, Regulations for Electrical Equipment of Buildings, obtainable from the Institution of Electrical Engineers, Savoy Place, London, W.C.2., price 6/-(paper bound), including postage.

The Mains Supply Cable

There are three ways in which we can run the cable from the house to the shed—ignoring such local variations as cleated wiring and insulator

supported tough rubber, now-frowned upon by many authorities.

First, the cable can be metal-sheathed and run underground, at a depth of at least 18in., (229 B(i)). This is perhaps the best method, but certainly the most expensive, and hardly suitable

for the job we are undertaking.

Second, the cable can be run through conduit, (229 B (ii)). Again, this is a satisfactory installation, providing the conduit is of the correct dimensions and properly earthed. But as this is only suitable for a comparatively short run, and there must be no joint in the conduit, and the problem of expense also arises, this method is not so attractive as the next.

Third, a catenary system. By this method, the cable is supported by a separate wire, isolated from the electrical circuit, (229 B (iv)). The wire that forms the catenary must be properly secured at each end, with the minimum of sag. For a short run, it is only necessary to bind the catenary wire to firmly anchored supports, then fix the power cable to it. A longer run may need some form of pulley at one end to strain the loaded catenary into a safe position when the traverse has been completed.

13A fused sockets can be used, (114 B) and if a sub-circuit is wired as a 'ring', up to 10 outlets can be connected to a 10A input, using 7/029 conductors. Allow a minimum of 100W per lampholder and a current of at least $\frac{1}{2}A$ at each 2A outlet.

Taking a practical example, for a small workshop that contains a single bench for radio and television repairs and experiments, we can subdivide the services as shown in Fig. 2. Here we have four separate lines, fed from a distributor board, each line fused, with a common switch that completely isolates the shed wiring. In addition, there is a fused switch at the house end, (112 A and B). The four lines are: Lighting.

Heating. Bench Power. Isolated supply.

The lighting, in this case, need only be a fluorescent fitting of some 40W, augmented by a bench-lamp, 60-100W. Total power requirements, 100 + 100 = 200W. (see above).

Heating can be provided by a single-bar space

heater of a maximum 1,000W. Use a 13A socket and at least a 10A fuse in the distributor



By Henry Maxwell

Binding the power cable to the catenary is, again, a matter for local specification. The general method, with PVC cable, or the toughrubber-sheathed (TRS) stipulated by the original I.E.E. Regs., is to bind the power cable to the catenary with a few turns of adhesive tape, and finish with a twist of galvanised wire. For 7/029 cable, the bindings must not be more than 9in. apart; for larger power cables, a 12in. spacing is used, with a 15in. interval on vertical runs, (210 C). Fig 1 shows the method described.

Choice of power cable depends on the expected load. For a typical small workshop, a 15A supply would be sufficient, for which 7/.029, twinplus-earth capothene covered cable would be suitable. For higher power loading, 7/044 can be used, capable of taking a 30A loading. If the earth wire is run separately, it must be capable of carrying three times the current of the fuse

rating, (Reg. 406).

Determining the Load

To calculate the loading, let each service that is wanted, i.e. lighting, heating, bench supply, etc., be reckoned as if the consumption was at the maximum.

For example, a full current rating should be assumed for a 15A outlet, (113) but for a consumption of between 15 and 30A several

Bench Power

Here we need a soldering iron, possibly two, one 25W or less for work on printed circuits and in confined spaces, and one of 100W for those occasional large jobs where the smaller iron is inadequate. The latter will only be plugged in when needed, but calculations must allow for it. There will also be a drill, again used only occasionally, and mains-powered bench instruments, such as the signal generator, oscilloscope, valve-voltmeter and stabilised power supply. Total power requirements, about 1,500W, with separate fused outlets and a common 15A fuse.

The isolated line feeds a 1:1 transformer of 250W rating, which supplies a number of outlets (for convenience), and is used for connection of the apparatus under bench test. The reason for this has been stressed often enough in these pages: universal, a.c./d.c. equipment has the chassis connected to one side of the mains input, and thus there is a danger of the operator completing the circuit to true earth via his body and receiving a shock that could at best be unpleasant; at worst. fatal. The distributor fuse will be 5A.

Switch-fuse

The switch-fuse, which should be mounted separately on a panel near the entrance and preferably at a height of at least four feet above floor level, will have a 15A fuse, and 7/.029 twin cable with 3/.036in. earth provides the power supply.

It will be noted that two multiple boards were mentioned in the above description. This is entirely a matter of choice. The author has fitted out several small workshops for his own use and found that the initial expense of a dozen different outlets is more than compensated by the later convenience. Nothing is more frustrating than

0 Mains 150W Lamps 52 20 amp. Water Heater Switch with Neon 2A 3p 15A 30 13A 15A 13A 3 p.flat Wylex 30 15W Lamp Earth BC 5A ampholder True earth

Fig. 3: Details of the series board.

having to remove and replace a plug for the sake of a five-minute test. Outlets are wired in parallel, with live and neutral poles correctly positioned and earth added where appropriate.

The Series Board

A refinement that is very little trouble to make, but can prove a great boon, is the Series Board

shown in Fig. 3.

Basically, this merely includes a couple of 150W lamps, with shorting switches, in series with the live line of the incoming mains. (In the case of the set-up of Fig. 2, this would be the mains from the isolating transformer.) When S1 and S2 are closed, the live line is continuous, and the outlets receive direct continuity. If S1 is now opened, the two lamps are paralleled and in series with the live line: thus, if a piece of equipment with a dead short-circuit is plugged into any of the sockets, the lamps will light to full intensity. If S2 is now opened, only the left-hand series lamp is in circuit.

The purposes of this board, apart from the protection against short-circuited equipment, cover the testing of motorised appliances, vacuum cleaners, drills, etc., of heaters, lamps, radio and television receivers. The single lamp position gives sufficient loading to test small motors, noting the regularity of illumination, which, with practice, can give an immediate indication of faulty brushes, commutators, and armatures. The double lamp position provides 300W in series with the appliance and is used for larger vacuum cleaners, washing machines, etc., and can be handy for indicating those sudden short-circuits in that would normally blow the television sets

Many applications will to the reader; testing fuses. occur flexible leads, acting in place of surge limiters for new electrolytic capacitors, checking double-load appliances, such as fan heaters and fires.

Earth Leakage Indicator

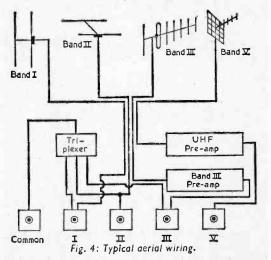
A small lamp in series with the earth lead, while retaining the safety aspect, acts as an indica-tion of earth leakage in a set or appliance. By fitting a take-off terminal on the 'hot' end of the lamp circuit, two-pin appliances can also be tested by connecting their casing directly to this point.

It should be noted that the system earth, as shown in Fig. 2, although carried through the whole of the wiring, is best augmented by a separate earth at the workshop end. A long earth can give protection against heavy leakage, but is very often a source of radio noise, especially noticeable when the receiver under test needs a good earth and aerial. This is understandable

when we consider that 11ft. of 7/:029 will give a 1V drop if a.c. is applied.

Aerial Installations

Much could be said about aerial installation for the small workshop, but all depends on the



amount of testing and experiment that is to be \ done.

Fig. 4 shows a sample of the aerial wiring for one 'den' that the author recently equipped. Note that the aerial leads (coaxial feeder) were brought in separately. Although more expensive, this method has definite advantages for the workshop, especially if signal strengths are to be monitored. The Band I and II signals were both sufficiently strong not to need pre-amplification, but Band III has its own pre-amplifier and the wiring is laid in for the u.h.f. band, although there is, as yet, no signal available.

One small refinement is the addition of a triplexer and 'common' aerial socket, which can save a lot of time when a television receiver is being tested. Changing leads every time the channels are switched can be frustrating—and does not do

the sockets any good either.

As a final note, remember that aerial feeders must be protected at the vulnerable points where they pass sharp edges, tiles, gutters, brick angles, etc. Fig. 5 shows a specimen run from rooftop through window-frame. Tile clips and gutter clips can be purchased quite cheaply, and a good, secure aerial installation pays for itself in the end.

It will, at least, enable the owner to sit and

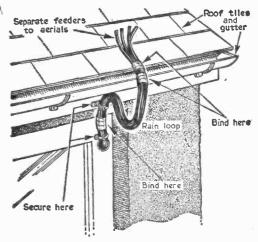


Fig. 5: Protecting aerial feeders.

view in comfort when those gales of winter come howling around again.



The Progressive

This receiver is built in successive stages, each new stage adding to the performance of the set and culminating in a six-transistor, two-waveband portable.

PORTABLE

By R. F. Graham

THIS receiver is particularly intended for beginners, because it can be made initially with two transistors only, in its original simple form, the extra stages being added one by one afterwards. As construction proceeds, there are thus only single stages to complete and test, and if any faults should be present, they can easily be located. As the receiver is developed, almost no changes have to be made to the sections already completed. The finished portable uses six transistors, and will give very good results.

As the receiver is a working unit from the very beginning, it is built in such a way as to accommodate the loudspeaker and battery, and the complete unit can be inserted intact in a suitable cabinet, without need to remove control knobs or any other items. It can as readily be lifted from the cabinet, for further constructional work.

When the receiver is out of its cabinet, it is so designed that it will stand upright, in the normal working position, so that it can be aligned and tested. It will also stand on either side, or may be placed flat, either way up, without any possible damage to components. This means that it can easily be handled, or turned over, while building is in progress.

As it is necessary to have components on both sides of the insulated panel, there is sometimes a little difficulty in checking leads which pass from one side to the other. To avoid this possible cause of wiring errors, a clear Perspex panel is used. All wires and parts can thus be seen from either side, and it is at once apparent where all leads go. The use of a transparent panel, in this way will be found very helpful.

To simplify wiring, etc., the set is first put into working condition for medium waves only, but the long wave band can be added at any time.

In the early stages of construction, the output is insufficient for a loudspeaker, so headphones are used. The receiver is, of course, very good indeed for headphone reception, and it may be desired to keep headphones, for personal listening, even when the output stage and loudspeaker have been added. It is also possible to add an external aerial, which is sometimes an advantage when the set is used in a screened locality, such as a vehicle. Running from a small 9V battery is also in order, though a large type 7½V battery can be accommodated, and has a very long working life.

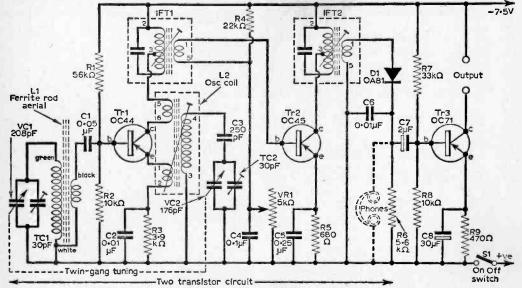


Fig. 1: The 3-transistor circuit for m.w. reception.

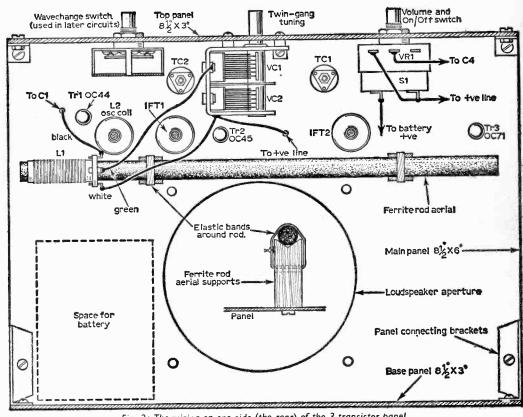


Fig. 2: The wiring on one side (the rear) of the 3-transistor panel.

Progressive Stages

Brief details of the circuits, in the order in which they can conveniently be used, are as follows:

(i) Two transistors, as frequency changer and i.f. amplifier, with diode detector. This allows the f.c. and i.f. circuits to be aligned and got into proper working order at the earliest stage. Volume is controlled by adjusting the i.f. transistor base voltage, and the set is for headphone reception.

(2) An audio amplifier is added, providing a three transistor circuit. This circuit gives very good headphone results, and the a.f. stage will later act as a driver for the output stage.

(3) A Class A output stage is added, making four transistors in all. This gives sufficient output to drive a loudspeaker unit.

(4) The second intermediate frequency stage is added, to obtain a five transistor circuit. The receiver then has a high degree of sensitivity, with good volume from quite a number of stations.

(5) The last transistor is fitted, giving a six transistor set with Class B push-pull output. This allows greater volume than the single transistor output stage.

(6) A long wave coil and trimmers, etc., are added, to permit both long wave and medium wave reception.

As mentioned, the set is complete, self-con-

tained, and in working order, through all the stages given above.

The Perspex Panel

The Perspex panel is 6in x 84in and \$\frac{1}{2}\$ in thick. The loudspeaker opening, \$3\frac{1}{2}\$ in diameter, is cut first. This is centrally placed and \$\frac{1}{2}\$ in from the bottom of the Perspex, as shown in Fig. 2. An adjustable washer cutter is most satisfactory, the cut being to about half depth each side. A fretsaw or similar saw could of course be used instead. It is also possible to drill a ring of holes, remove the centre disc, and clean up with a half round file, though this is more laborious. The loudspeaker is then rested in position, and the four securing holes are marked and drilled.

A line is drawn 1½in. from the top of the Perspex, and the oscillator coil and i.f. transformer are located along this line. The oscillator coil is 1½in. from the edge. The first i.f. transformer centre is 1in. from the oscillator coil centre, and it is 3in. from the centre of the first i.f. transformer to the centre of the third i.f. Assuming that the full six transistor receiver will be made eventually, the second i.f. will be fitted centrally between first and third i.f. transformers.

Hold the cans with the pins in the position shown in Fig. 3. The exact location of the pins

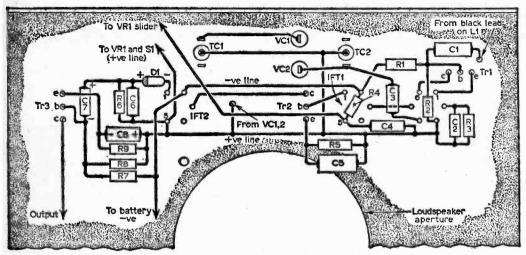


Fig. 3: The front of the panel showing the wiring.

will be seen, and can be marked with a sharp tool. Holes for the can tags and pins are then drilled.

Two mounts for the 8in, ferrite rod are made of insulated material, about 1½in, long. A groove is filed or cut to receive the rod, as in Fig. 2. Screws hold the supports to the Perspex, these screws being 2½in, from the panel top edge. Each support has a hole drilled through it, so that an elastic band can be placed round the rod, as shown. The ends of the band are joined with thread or a short piece of copper wire.

When the receiver is standing upright, out of its cabinet, it rests on a piece of 3-ply 3in x 8½in. This is held in place by the two brackets shown in Fig. 2. This piece of 3-ply also serves as a shelf to carry the battery.

The control knob panel is of Paxolin, preferably polished, and is also 3in. x 8½in. It is held by three small brackets, one each end, and one near the tuning capacitor, as in Fig. 2, Holes for the volume control and switch are 2in. from the panel ends.

To avoid hand-capacity effects, a piece of aluminium foil about 2½ in. x 6in. is cemented to the control knob panel, before fixing the volume control, switch, or tuning capacitor. This also serves to earth the bushes of the volume control and switch.

Holes are drilled directly over the capacitor tags. The control knob panel and 3-ply base should be fitted to the Perspex, as it is then possible to turn the receiver and rest it in any position. There is im space at the front of the panel, to accommodate capacitors up to in diameter.

To clarify wiring, it is a good plan to use red sleeving for all "earth" or positive circuits, and black sleeving for all negative circuits. Some other colour can then be employed for all the remaining connections. Tinned copper wire, of about 26s.w.g. will be found convenient throughout.

Three Transistors

As the a.f. amplifier is extremely simple, it is included in Fig. 1. To use the receiver with two

transistors only, omit Tr3, C7, R7, R8, R9 and C8, and wire the headphones in parallel with R6. Alternatively, it may be preferred to build the three transistor set at once. as any fault in the a.f. stage can at once be checked by connecting headphones across R6.

Thin coloured flex is soldered to the aerial winding tags, for easy identification. Black is one end of the base winding. Green is the tuned winding. Both windings are joined at one end, and the white lead is taken from this point.

Wiring of the rod aerial is shown in Fig. 2.

Wiring of the rod aerial is shown in Fig. 2. Black passes through a hole to CI. Green goes to the front section of the tuning capacitor. White is taken to the capacitor frame, and a wire passes down from the frame to the "earth line" in Fig. 3. The trimmers TC1 and TC2 are mounted by

The trimmers TC1 and TC2 are mounted by passing their tags through holes. Both centre tags go to the earth line, the remaining tags going to VC1 and VC2, as in Fig. 3.

Note that the white spot i.f. transformer is used in the first position, and the blue spot transformer in the final i.f. stage. All the can securing tags are joined, and serve as earth or M.C. connecting points, as in Fig. 3. Pin 4 on each IFT is unused, but should not touch other parts or wires.

There are relatively few parts and connections, and wiring should be quite easy. All transistor leads can be at least 1½ in. long. Solder these quickly, to avoid overheating. With the transistors mentioned, the red spot indicates the collector lead, shown by "C" in Fig. 3. The centre lead is the base, marked "B" while the remaining lead is the emitter, "E".

The diode and electrolytic capacitors should be connected in the polarity shown. The diode leads should be at least \(\frac{1}{2}\)in. long, and soldering should be completed rapidly.

If a receiver has never been constructed before, it will be very helpful to copy the circuit diagram in pencil. As a component is added, or a connection made, draw over the appropriate circuit elements in ink. There should then be no possibility at all of any mistake being made, and if a lead has been omitted, this will be obvious.

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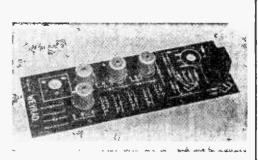
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R4 22k Ω R16 8·2k Ω	· · ·
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*R6 $5.6k\Omega$ R18 $3.9k\Omega$	TI Push-pull output transformer with 3Ω
R7 33k Ω R19 Ik Ω	secondary (Osmor)
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	Fig. I only)
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C13 18pF mica or ceramic	$8\frac{1}{2}$ in. \times $6\frac{1}{2}$ in. \times $\frac{7}{4}$ in. Hardboard 9 in. \times $6\frac{7}{2}$ in.
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C15 50μF electrolytic 15V C16 100μF electrolytic 15V	7½V battery (Vidor L5048, or Ever Ready AD38)
C16 100µF electrolytic 15V	The components marked * will not be required for
C17 180pF mica or ceramic VC1 208pF Two-gang variable with internal	the final 6-transistor receiver which will be des-
VCI 208pf I wo-gang variable with internal	cribed in a future issue.
VC2 176pF screen (Jackson 00)	Cripco in a fatare issue.
VC2 176pF screen (Jackson 00) TC1 30pF beehive trimmer	011141411 OF BEGINDENENES -000
TC2 30pF beehive trimmer	SUMMARY OF REQUIREMENTS FOR
TC3 60pF compression type trimmer	FIRST STAGE OF CONSTRUCTION
TC4 60pF compression type trimmer	Three Transistor M.W. Circuit (Fig. I)
Semiconductors:	Resistors: R1-R9, VR1
TRI OC44 TR4 OC72	Capacitors: C1-C8, TC1, TC2
TR2 OC45 TR5 OC45	Transistors: Tr1, Tr2, Tr3, D1
TR3 OC71 TR6 OC72	Inductors: L1 (m.w. winding), L2
(TR4 and TR6 should be matched pari)	Headphones (low resistance) are required for
DI ÖA8I diode	this circuit

Testing 3-Transistor Set

Medium or high impedance headphones, of moderately low d.c. resistance (say up to about 250 Ω) can be connected directly from Tr3 collector to battery negative. Do not leave Tr3 in circuit with nothing connected to the collector. For example if Tr3 is wired in, but the first two stages are to be tested by wiring phones across R6, join a $1k\Omega$ or similar spare resistor from Tr3 collector to battery negative.

Alignment follows usual methods, except that there are only two i.f. transformers. VR1 should be turned about one quarter way up only, and should be turned back, if volume is too great. It is easier to find accurate trimming positions when

volume is kept down.

With the three transistors and a $7\frac{1}{2}V$ supply, a meter in one battery lead should show about 4mA. If a signal generator can be obtained, align the

IFT's at 470kc/s, trim at 210m, and adjust oscillator coil core and aerial winding position at 500m.

Assuming that no signal generator is available, satisfactory adjustments can be obtained fairly readily, if the job is undertaken in the correct manner. The air-spaced beehive trimmers can be rotated with a length of ebonite tube, or similar material, cut at the end to engage the trimmer top. If compression trimmers are fitted instead, make sure these can open to a low capacity. For the coil and transformer cores, file a plastic knitting needle, or strip of insulating material, so that it will fit the core slots. Trying to work with a metal blade will only cause trouble (a suitable trimming tool is often supplied with these components).

If alignment is to be undertaken with no signal generator, first unscrew both trimmers TC1, TC2

-continued on page 669

A SIMPLE WAVETRAP

ELIMINATING ADJACENT STATION INTERFERENCE BY G. J. KING

A BIG medium-frequency reception problem is adjacent station interference. This is troublesome mostly after dusk and towards the high-frequency (low wavelength) end of the medium waveband. It manifests either as a whistle or whistles of varying intensity as the wanted station is tuned in and the tuning control is adjusted in an endeavour to clear the background of so-called "monkey chatter".

How the Interference is Caused

Whistles are caused by nearby unwanted signals beating with the wanted signal. When there is only one unwanted signal within audio distance of the wanted signal the two signals produce a troublesome third signal. Let us suppose that the interfering signal is, say, 2 kc/s away from the wanted signal. No ordinary domestic receiver could possibly discriminate between such closely spaced signals, so such a receiver responds to them both.

They both arrive at the detector whose nonlinear function cause one of them to be modulated upon the other, and it is here that a signal at the difference frequency is created. This signal "looks" to the rest of the set like true audio—which, of course, it is—and it thus gets through the receiving circuits along with the modulation of both the

wanted and unwanted signals.

A 2 kc/s whistle is thus superimposed upon the wanted audio and the unwanted modulation and extremely distressing interference results. As each station is fixed in frequency the frequency difference always remains the same and the whistle holds at its original pitch even when the tuning control is adjusted. All that happens is that the intensity of the whistle varies as both signals are brought within the embrace of the receiver response.

Several whistles at different pitches result when more than one interfering carrier or signal falls within the passband of the receiver, but on most modern superhets the response to signals removed by about 6 kc/s or more from the wanted signal is so small as not to cause trouble. Moreover, even if a 6 kc/s plus beat found its way into the audio section very little output would result owing to the treble limitation of the majority of domestic audio

sections.

This is not meant to be derogatory of design, but simply to illustrate the wastefulness of designing for a wide audio passband when it could never be used on the medium frequencies owing

to adjacent station interference problems. In radiograms and models with v.h.f.-f.m. facilities, of course, an extended audio section is extremely desirable, but even so quite a bit of treble cut is demanded to reduce the annoyance value of whistles when working at the top end of the medium waveband — such as on Radio Luxembourg.

Monkey Chatter

Monkey chatter is the effect which is produced by sidebands of an unwanted modulated signal breaking into the narrow spectrum to which the set is tuned. It can be demonstrated by carefully detuning, say, the l.w. Light Programme of the BBC when a good quality "live" programme is being broadcast. As the set is detuned away from the carrier so only the sideband signals of the transmission will be heard, and as the detuning is continued only the high order sidebands produce an output as they "splash" into the receiver's response. Transistor portables are ideal for demonstrating the effect owing to the relatively sharp cut-off characteristics of transistors.

Thus, in addition to whistles, adjacent stations produce monkey chatter symptoms and the combined effect, especially when it is related to several interfering signals, can be very disconcerting. The BBC's solution to the problem, of course, is v.h.f.-f.m. transmissions in Band II, and where possible these should always be used for local programmes. However, the medium frequencies still have to be employed for more distant stations and for Radio Luxembourg, so it is worth while to explore the possibilities of, at

least, alleviating the interference effects.

Series-Tuned Rejector

What is wanted is some means of putting a sharp, narrow trough into the overall response curve at the interfering frequency point; but before we go into that let us investigate the overall response curve of an average receiver. Such a curve is depicted in Fig. 1. The overall response extends pretty well 12 kc/s either side of the tuned frequency, but at that displacement the response is zero so an interfering station 12 kc/s away from the carrier would not cause any trouble. In any case, it is unlikely whether the set would give an output at 12 kc/s (as this is very high audio).

However, at 6 kc/s either side of the tuned

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frequency the response is about 50 per cent of maximum. This is essential, of course, if the medium frequency audio sidebands are to be retained and there is not to be too much treble suppression in the r.f./i.f. stages of the set. This means, therefore, that any interfering signal displaced up to, say, 6 kc/s from the tuned frequency will cause a response or output,

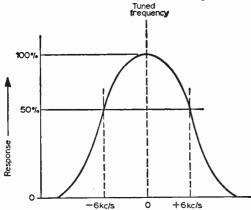


Fig. 1: Response curve of an average receiver. An interfering signal about 12kc/s away from the tuned frequency would not cause any trouble, but a signal 6kc/s away would result in a 6kc/s whistle due to beating as explained in the text.

Now, if the response is narrowed still further, as shown in Fig. 2, although the response to interference 6 kc/s either side of the tuned frequency is only about 5 per cent (26dB down), treble sidebands of the modulation would also be suppressed by the same amount and the reproduction would be very poor indeed.

Suppression of the order of 26dB is not sufficient to "kill" the whistle effect completely, though it goes a long way towards minimising it, and if the treble response of the set is down audio-wise at

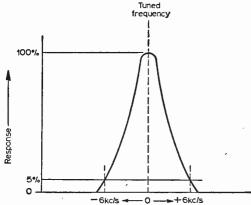


Fig. 2: If the overall response is narrowed as shown here the sideband components of the modulated signal would be severely attenuated and bad treble cut would spoil the reproduction. This is not a solution to the problem of adjacent station interference.

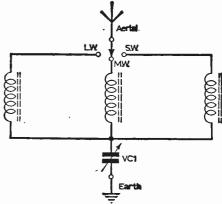


Fig. 3: A simple series-tuned wavetrap or rejector circuit. The coils should have a Q value of preferably not less than 250 and the capacitor should have a maximum value of 500pF for all-wave use, 300pf for m.w. use or 100pF for s.w. use. Connection should be either across the aerial and earth sockets of the set (across the operating frame aerial or ferrite rod winding in the case of a portable) or between the metal chassis of the set and the signal grid on the frequency changer valve. On a.c./d.c. sets capacitive isolation is essential to avoid the risk of electric shock.

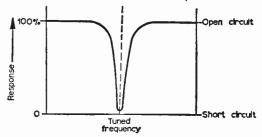


Fig. 4: The type of trough introduced by the rejector.

6 kc/s, then the two attenuating factors together would amost certainly eliminate the disturbance; but narrowing of the overall response is not generally a practical way out of the trouble.

If there is only one interfering signal, the resulting whistle can almost certainly be cleared by a high-Q series-tuned rejector of the kind shown in Fig. 3. Such a rejector "looks" to signal at the tuned frequency as pretty well a dead short, while to signals at frequencies outside the narrow response there is virtually zero attenuation. The idea is shown in Fig. 4.

To get the system to work, the narrow response of Fig. 4 must be superimposed at the point of interfering signal upon the response of Fig. 1, as shown in Fig. 5. Here it is supposed that the interfering signal is plus 4 kc/s away from the wanted signal. Thus, the flylead of Fig. 3 would be connected to the appropriate coil or coil section and VC1 would be adjusted until the rejector is tuned exactly plus 4 kc/s from the wanted signal. As VC1 is tuned over the wanted carrier, the signal would dip, would then rise and close by would be a point where the whistle would disappear almost completely—how well depending

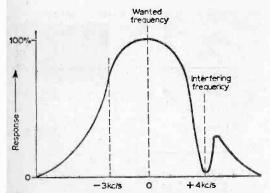


Fig. 5: Here is shown the rejector adjusted to suppress an interfering carrier plus 4kc/s from the tuned frequency of a receiver. The degree of attenuation to the unwanted signal given by the rejector is governed by the efficiency or Q value of the circuit.

upon the efficiency, or Q value, of the rejector circuit.

If there are several whistles, it is not feasible to employ a number of rejector circuits as they tend to interact with each other, and unless the circuits are expensively designed it is virtually impossible to improve matters. Nevertheless, even with several whistles, quite a relief is secured by getting rid of the strongest one.

Connecting the Rejector

The rejector circuit is often best connected between the aerial and earth sockets of the receiver or tuner, but if this results in too much loading across the circuit and a reduction of effective Q. the combination can be tried between the signal grid of the frequency changer valve and the metal

chassis of the set.

It is perfectly in order to use the rejector with portable sets. Here it should be connected to chassis on the capacitor side of the rejector and to the slider of the aerial wavechange switch on the other side, so that irrespective of waveband to which the set is tuned the rejector is always effectively across the operating winding of the frame or ferrite rod aerial. On a.c. d.c. receivers care must be taken to prevent electric shock—particularly to the uninitiated and the young in the family—and no connection whatsoever should be made direct to chassis. 250 volt a.c. working capacitors of not greater than 1,000 pF should always be used for isolation.

Construction

Construction is very straightforward and needs little comment. The rejector can easily be housed in a coffee, cocoa or tobacco tin. The capacitor and coils should be mounted inside with an outside knob for tuning and a couple of sockets or terminals for connecting to the set.

With an all-wave (or long wave and medium wave) version it is desirable to employ a simple wave-change switch to avoid having to alter coil taps when changing band. Mainly, however, the device is designed to tune the medium waveband

only, in which case a high-Q medium wave coil and a tuning capacitor (preferably air spaced) of $0.0003\mu F$ are required. Suitable high-Q coils and capacitors are readily available from most of our component advertisers. The coil should have a Q of 250 or so.

The rejector has been used in conjunction with a high-quality a.m. tuner-to climinate most of the mush and whistles around 208 metres with considerable success.

For Television

A similar rejector for suppressing pattern interference due to an unwanted carrier close to the vision frequency on Band I channels can be made along similar lines. A suitable circuit, with construction details, is given in Fig. 6.

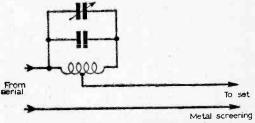


Fig. 6: A simple TV rejector circuit for clearing pattern interference produced by an interfering r.f. signal within the vision passband. The coil is 2 turns of 18s.w.g. tinned copper wire, \$in. diameter, self-supporting, tapped at ½-turn from aerial end.

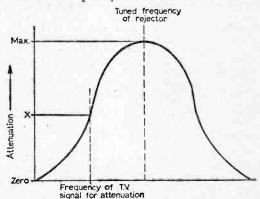


Fig. 7. Showing how the rejector of Fig. 6 can be used as a signal equaliser. Point X on the curve reveals the degree of attenuation.

The idea can also be extended for equalising the signals in Bands I and III at the end of a television downlead. Usually the Band I signal is several times stronger than the Band III signal, meaning that the Band I signal requires a few decibels of attenuation relative to the Band III signal. By using a rejector of the type shown in Fig. 6 is can be adjusted on the Band I channel to introduce sufficient attenuation as to balance with the Band III signal, as shown in Fig. 7. Here the rejector is tuned to one of its sloping sides until the required degree of signal attenuation is introduced.

Infra-Red I Heaters Make up one of these latest type heaters ideal for bathroom, etc. They are simple to make from

our easy-to-follow instructions. uses silica enclosed elements designed for the correct infra-red wavelength (3 microns). Price for 750 watt element and metal casi as illustrated 19/6, plus 2/6 post and insur-

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Waterproof heater wire, 16 yds, length, 70 watts. Self-regulating temperature control. 10/-, post free.

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Single and 2-gang types size with good length spindle, all new and boxed. Single types, 1/- each, values available: 5K 10K, 25K, 50K, 100K, 250K, 1 meg., 2 meg.

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American made. Dyna-mic type. Real bargain Dynamic type. Real bargain at 3/6, plus 6d. postage.

Crystal type 5/6.



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As supplied to many schools and colleges. A simple basic superhet easy to un-derstand and which can be progressively xtended.



extended dideal for students—components include valves—metal rectifier tuning condenser—1.F. transformers, etc. In fact complete superhet except speaker. Price 23 plus 3/- post and insurance. Data included free or sep. 1/6.

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is available this
month at a
special snip price
of 12/6, plus 3/6
post and insurance. Bize is 131in. x 9in. x 4in. and it is nicely covered in two to tone

Bargains For Callers

We always have plenty, e.g. T.V. Cabinets, ideal for shelves etc., 2/6 each.

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Made for a famous company intending to make a Battery Record Player but changing their minds. This is an extremely fine looking cabinet, must have cost at least £2 to make. It is complete with handle and fasteners as illustrated. Also included in the parcel is a Cosmocord pick-up with crystal cartridge and sapphire stylus. Both items new and perfect. Only 19/6, plus 4/6 post and insprance





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This Pocket Secretary could eliminate the trouble (often embarrass-



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Specifications: Dimensions: 61 x 21 x 14m. Weight: 14 oz. Recording time: 12 mins. rewinding time 4 mins. Recording system: D.C. Bias. Erasing system: Magnetic erasing, wow and futter: Within 2%, and frequency response: 500-1,200 c/s (within —6db).

Price \$9.19.6. Complete ready to work.

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recorder at a "give away"
price. The tape recorder has
not been used but may be
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sell it for its apares value only.
It contains among other
things: Tape head, suitable
for dual track working.
4 transistor push-puil amplifer.

transistor push-pull amplifier taps motor with pulleys and drive mechanism, volume control, record—erase—playback—off lever action switch. All assembled in a plastic case with carrying handle. Every item listed above is warranted in good working order and if not so, will be replaced free of charge. free of charge.

The whole offered at less than the value of the amplifier alone, namely 45/-, plus 2/6 carriage.

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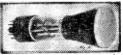
Kit of parts comprising; choke, two lamp

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AUDIO LEVEL INDICATOR

By C. MORGAN

A directional aid for setting up microphones and loudspeakers

THE noise level indicator described in this issue was developed mainly for the setting up of a recording studio. Since then many other practical uses for this very versatile indicator have been discovered. Some of the uses have been to test the sound absorbed by certain materials in use in the studio, setting up of the loudspeakers in a display field so that all sections of the audience receive good information (badly needed in certain open-air displays) and laying out of the stereo loudspeakers to get the best effect possible.

Other applications include the monitoring of recordings, thereby dispensing with the monitoring headphones, leaving the ears free, and enabling the operator to stop the recording when the sound

level is too faint to be recorded. It can also be used with an extended microphone on an umbrella to give a directional effect from one position only.

Although sound reflectors are available the price may be beyond the pocket for some enthusiasts, but if an old umbrella is pressed into service, with the microphone positioned as shown in the drawing (Fig. 4), a very directional effect can be produced. This is so effective that the writer has abandoned his solid reflector in favour of a small umbrella which is very portable, takes up little room and can be stowed away when not in use.

The Circuit Construction: Sound Amplifier Stage

The microphone is of the moving-coil variety, the one in use being an ex-Army hand-set type which requires the use of a step-up transformer. If the intending constructor does not wish to use a moving coil type a crystal type will work just as well but due to the higher output the step-up transformer will not be required.

The output of the transformer, or the crystal microphone, is fed into a two-stage transistor amplifier, the output of which is coup-

led to a rectifier into a moving-coil meter. The battery supply is 9V, miniature deaf aid type.

No special requirements are specified as to the layout of the wiring, except to keep the connecting wires of the transistors cold when soldering them into position. The use of heat shunts, in the form of a pair of flat-nosed pliers, will suffice.

The mounting of the battery is simplicity itself. Two small pieces of thin, thick paxolin were obtained from a run-down 90V battery, the brass clips were taken from a 4½V torch battery and bent to suit. These were then clipped to the paxolin with paper staples and a blob of solder placed on each one and marked (-) and (+).

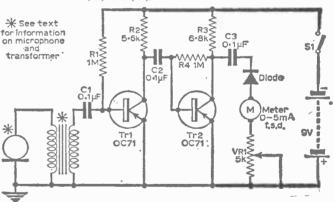


Fig. 1: The circuit diagram.

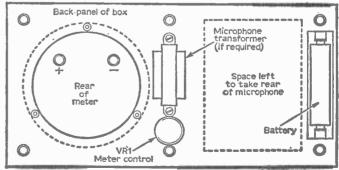


Fig. 2: A view of the assembled unit.

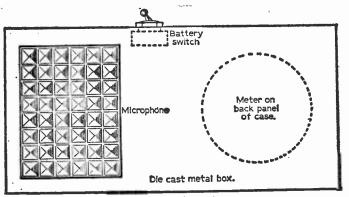


Fig. 3: Details of the front of the case.

The second piece of paxolin was then fitted, two pieces being held in place while the holes to take two self-tapping screws were drilled. The reason why two pieces of paxolin were used is to prevent the connections to the battery (carried by the top piece) shorting out to the case. If the level indicator is to be used with other than gentle hands the battery can be taped into position.

Using the Umbrella as a Sound Reflector

Two types of umbrellas were tried out, the first being a large conventional cloth one. This had a marked directional effect but a lot of sound was lost due to the porosity of the material covering the frame. Painting the inside with a silver paint reflected the sound rather better but also reflected the sun's rays so well that it damaged the plastic container of the mike.

Anyone intending to experiment with the sole purpose of solar heat in mind will have no difficulty in obtaining heat in the order of 112°C+.

The second type of umbrella tried was an Empire one of conventional size, the diameter being only 2ft 6in. across. It is made of plastic, which is an almost perfect medium for reflecting sound, and unless coated with a surface reflecting

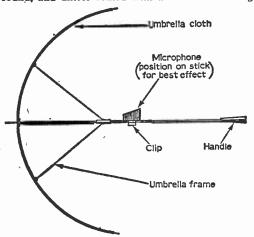


Fig. 4: Details of the modified umbrella.

paint will not damage the microphone.

One other very good point in favour of the Empire umbrella is that the rod supporting the ribs, etc., is made of hollow light metal. When the sound focal point has been found in the umbrella (about 5in. from centre) the handle and the point that projects through the frame can be sawn off. The micro-phone leads can then be fed through the rod and in that way making a far neater job.

If a in. diameter "Terry" clip is secured to the microphone with the assistance of a small self-tapping screw the microphone can be slid along

the rod to widen or narrow the sound angle.

If, then, the termination of the microphone is plugged into the noise level indicator, and the reflector is beamed on to a distant sound, the meter will indicate when the maximum sound has been obtained.

COMPONENTS LIST

Resistors:

6.8kΩ RI $\mathsf{IM}\Omega$ R3 5-6kΩ **R4** $IM\Omega$ R2 VRI 5kΩ miniature potentiometer RJ-R4 are # watt

Capacitors (paper): Cl 0·lμF C2

0·1µF $0 \cdot l \mu F$

Semiconductors:

TRI OC71, or equivalent OC71, or equivalent Tr2

Any suitable germanium diode

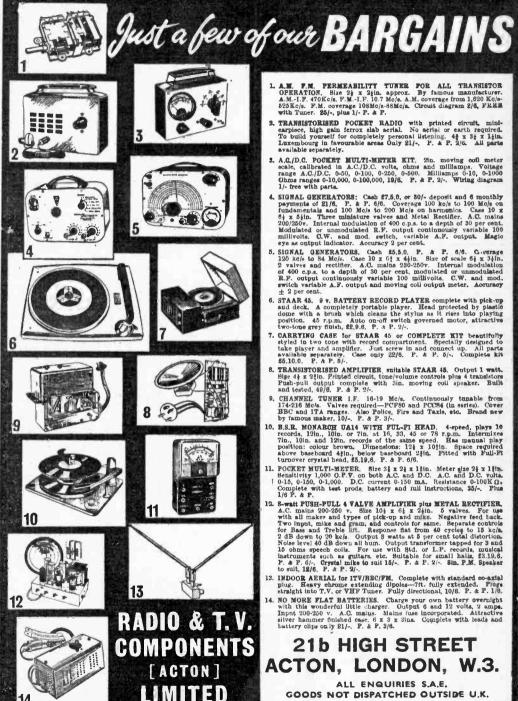
Miscellaneous:

Moving coil microphone and matching transformer. Die cast metal box to suit either internal or external microphone, as desired. Indicator knob and reference dial marker. 9V deaf-aid battery. Paxolin and brass connectors. Selftapping screws. Insulated connecting wire, etc.

This set-up can also be used for the transmission of sound in mainly one direction only. A miniature (2½in.) loudspeaker was installed in place of the microphone and connected to the tape recorder extension loudspeaker socket. A microphone was set up at a distance of 100yd, using the described noise level indicator.

The loudspeaker was placed into position approximately in the centre of the umbrella and then pointed in the direction of the indicator, when maximum signal reading was obtained in that position. The loudspeaker was then moved in and out of the umbrella and a position was obtained on the rod where, if the reflector was taken away, a loss of two-thirds of the total volume was indicated.

-continued on page 662



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 Noise level 40 dB down all hum. Output transformer tapped for 8 and
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 P. & P. 0'-. Crystal mike to suit 15/-. F. & F. 2/-. 8in. F.M. Speaker
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- 13. INDOOR AERIAL for ITV/BBC/FM. Complete with standard co-axial plug. Heavy chrome extending dipoles—7tt. fully extended. Plugs straight into T.V. or VHF Tuner. Fully directional, 10/6. P. & P. 1/8.
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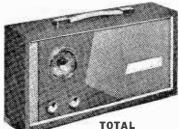
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PART 9 OUTPUT METERS AND THE G.D.O.

H. W. Hellyer

To was the intention, at the outset of this series, to devote the final article to a fleeting review of the rarely used instruments that augment such test gear as has already been described. In particular, the output meter requires brief discussion. The various forms of bridge. Q-meters, transistor testers and waveform oscillators and the handy but little-used G.D.O. were covered in

my original synopsis.

But the Editor has pointed out that many of these instruments have been discussed in these pages, and in *Practical Television*, either in constructional articles or during the course of description of more elaborate gear. For example, the Grid-Dip Meter is covered to some extent in an article by A. W. Hartley, in *Practical Television* for August 1963; F. G. Rayer's article on "Amateur Band Frequency Checking" in the September issue of this magazine brings in some valuable information on Absorption meters and Crystal Calibrators: articles by J. H. B. Gould, currently appearing, deal with adjuncts to the oscilloscope, timebases, a.c. amplifiers, square

wave generator, etc., as have also the previous series on oscilloscope design by M. L. Michaelis in both magazines, and some handy practical notes on these can also be referred to in *Practical Television*, January 1961, "Oscilloscope Faults", by W. Cleland, as well as in the more recent constructional series "The Henlow Wide-Band Oscilloscope", by D. R. Bowman, (*Practical Television*, June—October 1963).

In the April issue of this magazine, R. P. Hubbard described "A Cathode Ray Level Indicator", with application as

visual signal tracer, a.c. bridge null indicator and G.D.O. absorption indicator. The May issue brought us a "Miniature Test Oscillator" by R. Leyland and a "Pocket Signal Injector" was covered in the July issue by R. W. Kneeshaw.

Regular readers will need no reminding of the many other instruments that have been dealt with in past years. My aim, in this concluding article of the series, will be to concentrate on two types of instrument only: the output meter, and the griddip oscillator.

Output Measurement

Too often, during alignment, the engineer or contructor "short-circuits" the approved method and uses his ear as an output monitor, instead of the vastly more accurate output meter.

Whereas the human ear is a fallible—even gullible—instrument, which reacts to changes in intensity at different efficiency, according to the pitch and relative loudness of the sound, and varies widely between individuals, the meter can give a much more accurate assessment of power levels and their small variations. Even the simplest setup of an a.c. meter across the secondary of the audio output transformer will give us a quicker indication of sound intensity changes than we can hear for ourselves. And remember, absolute accuracy of power output is not essential for general alignment: normally, we are adjusting tuned circuits for a maximum reading, and the actual figure on the dial need only be a relative one.

In practice, the sound of a tuning note can become terribly wearisome, and it is better to disconnect the loudspeaker. When this is done it is necessary to provide a dummy load so that the output transformer "sees" the correct matching. Failure to do this will generally end with the screen grid of the output valve glowing red-hot.

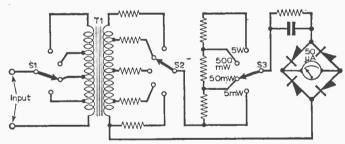


Fig. 1: Circuit of a commercial high and low output meter. S1 is the impedance multiplier, S2 the impedance selector and S3 the meter multiplier.

T1 is a tapped a.f. transformer.

Although the meter across the secondary may be thought to be sufficient load in itself, it is nevertheless good practice to shunt a resistor of the appropriate value across the secondary, taking off the a.c. voltage variation with the meter. It should be remembered, too, that output meters usually have variable impedance tappings, and many are suitable for connection to the primary of the output transformer (via a d.c. blocking capacitor, say $0 + \mu F$). The circuit of a typical meter of this style is shown in Fig. 1.

A tapped transformer is incorporated, with multiplier tappings, augmented by wire-wound resistors, in the primary winding, and an impedance selector switch in the secondary. A meter multiplier feeds the bridge circuit, allowing the meter, which may be a 50 A movement, to read

off rectified d.c. as output values between 5mW and up to 5W. This type of instrument gives accurate readings for comparative measurement over a fairly wide frequency range. An example of quoted specifications: level within 1dB (±) from 50 to 10,000c/s.

The Decibel

646

Having mentioned decibels, it may be as well to deal briefly with their use. Several articles on the decibel have appeared in these pages and it is not intended here to waste too much space on basic theory; but as the alignment data published by manufacturers usually states output in dB, some notes may be applicable.

The decibel is a ratio, either between two powers or two voltages. It is important not to

confuse the two quantities.

The power ratio is based on the fundamental sensitivity of the ear. When volume is increased, the impression relayed to the brain is proportional to the logarithm of the ratio of the energy of the sound levels. The common log of the two powers gives their relationship in Bels. The Bel is too clumsy a unit, however—the whole range of human hearing from the threshold of hearing to the threshold of pain is covered by only 13 Bels, so this device is divided by ten, becoming the decibel.

Mathematically, N dB=10 log 10 (P2/P1), where P1 is the input and P2 the output power. More practically, P1 may be the first reading, and P2 the second reading, when an alteration in input

to the amplifier is made.

For example, suppose the receiver is supplying 1W to the loudspeaker with a specified input, and this input is increased until the output is 2W. We could say the output has doubled, but it would be more accurate (to measure intermediate changes also), to specify a 3dB increase. In actual fact, the figures do not work out quite so neatly, and the increase is really 3.01dB.

Halving the power would give a 3dB decrease, or, a change of -3dB. As our meter gives a readable indication of fractions of a decibel and the smallest change in sound intensity that our ear will discern is about 1dB, depending upon the character of the sound, it becomes apparent why alignment with the aid of an output meter is preferable to judgement of power level with the ear alone. For example, a normal "quiet" listening level of 1.9W increased to 3W gives a 2dB change, readily noted on the meter scale but quite difficult to judge accurately with a single tone of say, 400 cycles, which is modulating the signal generator input.

Voltage and Current Ratios

This ratio, the decibel, is also extensively used for comparison of voltages and currents, but must not be confused with the *power* dB scale of our output meter.

For voltage comparison, it is necessary to specify the resistance across which the voltages are taken. Where the resistance is the same NdB=10 log 10 (V2²/V1²).

Remembering that a number squared is equivalent to its logarithm X2, we can express this as

 $NdB = 20 \log 10 (V2/V1)$.

Where receiver sensitivity is being considered, we are concerned with this ratio, the gain of a stage being the increase of the output on the input.

Thus, we can speak of a stage having 20dB gain, meaning that the output is 20dB up, compared with the input, or a ratio of 10:1 (for an input of 0·1V, an output of 1V is obtained. Similarly, a 20dB attenuator would decrease 1V by 10 times, or to $\frac{1}{10}$ V.

Other useful ratios are 10dB, actually 3:162 to 1, but near enough 3:1 for normal purposes, and 6dB, the ratio of 2:1, which is widely used in

audio work and alignment.

The usefulness of the decibel comes into play when we consider the added gains of several stages. Instead of unwieldy multiplication or division sums, we simply add or subtract the dB ratios. Thus a three-stage amplifier with stage gains of 2, 3 and 10 would have an overall gain of $2 \times 3 \times 10 = 60:1$. In dBs, this becomes, 6+10+20=36dB.

From the foregoing, it is obvious that to say an output is 10dB means nothing unless we relate our figure to the input. For alignment purposes, a reference output of 50mW may be used, and dB ratios are calibrated on the output meter scale above and below this reference point.

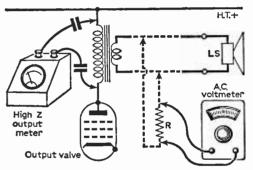


Fig. 2: Methods of connecting the output meter.

Using an A.C. Voltmeter

In practice, it is often desirable to use the output meter across the primary of the output transformer, suitably isolated, as shown in Fig. 2 in which case a direct wattage reading or dB measurement is obtained. The method used in cases where only occasional check on output has to be made is to connect a multimeter, switched to its 0-10V a.c. range across a resistor which is fitted to replace the loudspeaker, or simply across the transformer secondary, leaving the loudspeaker in circuit. The resistor should be equivalent to the impedance of the transformer secondary and preferably wirewound, to handle the wattage. To calculate this wattage, divide the square of the measured a.c. voltage by the resistance of the output, thus $W=V^2/R$. For example, an indication of 3V across a 2.5Ω load represents a power output of 3.6W.

Transistorised Equipment

Alignment of transistorised equipment sometimes needs a different approach. Output circuits have been developed which employ no output transformer. To disconnect the loudspeaker of such a circuit is impractical, and the meter should be connected across the loudspeaker speech coil as shown in Fig. 3(a) and (b). A 50Ω speech coil

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needs the meter switched to its 5—10V a.c. range, and a 5Ω loudspeaker requires a range of 1—2V a.c. for the most accurate readings.

An alternative method is to insert a d.c. milliameter in the battery lead, as shown. The quiescent current of the average set would be between 7 and 10mA, and the current at average listening level from 15 to 25mA. This depends upon the receiver, and reference should be made to maker's specifications when in any doubt.

Grid-Dip Oscillator

This instrument does not receive much use in the radio service department, for the obvious reason that it is quicker to replace a coil than to rewind it, and easier to trust the manufacturer's design of tuned circuits than to modify them in the course of repair. But the amateur is in the happier position of having plenty of time to experiment—and it is worth remembering that in the history of radio, it is his experiments that have brought about the majority of advances. Whereas

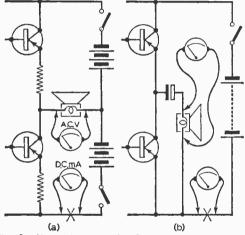


Fig. 3: Alternative methods of transistor output stage measurement.

the position may have changed in the field of television and advanced electronics, where experiment is an expensive business (although not entirely closed, as a survey of our companion magazine, *Practical Television*, will show) there is still plenty of original work going on in the audio field.

From the foregoing remarks it may be thought that the G.D.O. is very much a home-constructed instrument. In fact, there are several quite elaborate pieces of test gear on the market. Typical of the general-purpose design is the Q-Max GD02. This retailed (in 1960) at 15 guineas, with extra coils at 7s. 6d., and covered a frequency range of 1.5 to 300Mc/s with eight plugin coils. The circuit was built around a double, triode valve, one half as a Colpitts oscillator, the other as h.t. rectifier. The tuning capacitor is driven by a 5:1 slow motion drive, with hair-line cursor, direct calibration and a logging scale. It is mains powered and can be used as resonant frequency tester, in the normal way, as obsorption wavemeter, phone monitor (a jack is provided), oscillating detector and simple signal generator.

Another popular model, covering a 1.7 to 250Mc/s range, in six steps, is the Grundig 701. A four-position switch changes the function of the instrument to (a) a receiver supplying an a.f. signal to a pair of phones; (b) a wavemeter; (c) standard grid-dip oscillator; and (d) modulated signal generator.

Reference to the August 1963 issue of *Practical Television* will show how readily the G.D.O. design can be made up into a practical unit. A. W. Hartley has given explicit constructional details, and it is not my purpose to repeat his information. The following notes on basic design and applications should prove that the G.D.O. is a useful and comprehensive instrument.

Design Details

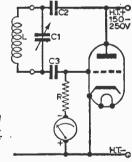
Whereas the Colpitts oscillator is considered more suitable for a wide frequency range, the alternative simple circuit, as shown in Fig. 4(a), employs a Hartley oscillator and may be more readily constructed from the spares box.

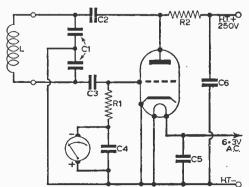
This circuit is deceptively simple. The valve used in the prototype was a 955, but other convenient triodes could be employed. The one component that requires special selection is the capacitor C1, which is a 5pF air-spaced variable with an insulated shaft. C2 and C3 are ceramic capacitors, 50pF and 25pF respectively, R1 is $18k\Omega$, and L is four turns of 16s.w.g. silvered wire on a $\frac{1}{2}in.$ low-loss former. Spacing and spreading the coil turns gave a coverage of 150-200Mc/s with a quite good indication of resonance on the $500\mu A$ meter movement.

Fig. 4(b) shows a little more complicated design that had to be developed to widen the range from 130-270Mc/s. C1 was a 35-35pF split stator,

C2 and C3 are both 50pF ceramic, and the decoupling capacitors, C4. C5 and C6 are all 1.000pF ceramics. R1 is $22k\Omega$ and R2 is $68k\Omega$. The coil is simply $1\frac{1}{2}$ in. of silvered 14s.w.g. bent into a $\frac{1}{2}$ in. U-shaped loop.

Fig. 4a (right): Hartley and b (below) Colpitts oscillators used as basis of G.D.O.'s.





Calibrating the G.D.O.

Calibration can be carried out in several ways. For high frequencies it is necessary to make up Lecher wire transmission line, which can be two parallel wires of 18s.w.g., insulated at each end from their supports and spaced 2in. apart, fixed as taut as possible.

A single turn loop is soldered across one end of the pair of wires for coupling to the G.D.O. and a knife-edge metal shorting bar placed across the two wires at right angles to alter the length. The coil of the G.D.O. is held close to the loop of the Lecher wires and the shorting bar slid along until a position is found where the grid current reading on the meter dips. The bar is moved along again until another dip is noted. The distance between the two dips is half a wavelength, and the G.D.O. resonant frequency is calculated from the formula

f (in Mc/s)=
$$\frac{150}{\text{distance}}$$
in metres, or 5905

distance in inches.

This method is suitable for laboratory work but as length of 40ft or more may be needed, is not practical for the amateur, who may prefer matching the G.D.O. resonant frequency to a known standard from a signal generator or received

signal.

First, tune the receiver accurately to the frequency estimated. Note the tuning of known signals and scale off the difference, making allowance for discrepancies of the dial, etc. Better still, inject a known signal from a crystal oscillator or signal generator and listen for zero beat at marker frequencies. After tuning the receiver accurately, couple the G.D.O. loosely to the aerial input circuit and swing the tuning capacitor of the G.D.O. until zero beat is obtained with the marker switched off—that is, with the G.D.O. used as heterodyne frequency meter. Keep the receiver gain down and check for the position of maximum response, to avoid confusion with image frequencies. For further information, refer also to the method used by Mr. Hartley, page 508, August 1963 Practical Television.

G.D.O. Applications

The principal use of the G.D.O. is to determine the resonant frequency of a tuned circuit. This is

performed as follows.

First, insert a coil covering the possible range, switch off the receiver under test, to prevent damping of the tuned circuits by the grid-cathode capacitance of valves. Couple the G.D.O. loosely to the circuit under test and tune for maximum dip. Too tight a coupling will cause the meter reading to pull and experiment will be needed. Check also

References

Radio and Television Test Instruments, by Gordon J. King.

Television Receiver Servicing, by E. A. W. Spread-

Radio Laboratory Handbook, by M. G. Scroggie. Admiralty Handbook of Wireless Telegraphy,

The Practical Radio Engineer, Vol. 16, No. 3. Radio Retailing, Vol. XV, No. 9.

that spurious results are not obtained by unwanted coupling with adjacent circuits by short-circuiting the tuned circuits individually and noting that the wanted one should upset the G.D.O. meter reading most.

If connections are not easily reached, the tip of a pencil touched on the "live" circuit connections will give quite observable results. If the circuit under test is completely screened, it may be desirable to leave the can in place, and an auxiliary coupling can be made with a piece of p.v.c. wire, twisted around one terminal of the G.D.O. coil and the "live" terminal of the tuned circuit. The wire should be twisted around these points with only its insulation touching, not making a direct connection.

To check closely coupled circuits, such as i.f. transformers, fit a swamping resistor, about $10k\Omega$, across the circuit *not* under test. Check by the

pencil test as stated above.

Testing r.f. chokes and capacitors is best done by short-circuiting their ends and loosely coupling the G.D.O. An open-circuit choke will give an indication of its parallel resonance, a short-circuited choke, its series resonance. Capacitors used as bypass components in r.f. and i.f. circuits may act perfectly well as capacitors but have unwanted inductive effects at the higher frequencies, and if the short-circuiting connections are approximate to the length of the connecting leads in situ the G.D.O. will enable us to judge at what frequencies these inductive and capacitative effects cancel, giving the optimum bypass.

To measure inductance, connect the coil across

To measure inductance, connect the coil across a capacitor of known value and loosely couple the G.D.O. tuning for a dip. Then the inductance in microHenries=

25,300

 $C (pF) \times f (Mc/s)$

To measure capacitance requires a calibrated variable capacitor to first tune an appropriate coil to a frequency determined by the G.D.O. setting. Then the unknown capacitor is connected across the variable and again a frequency measurement taken. The difference in the two settlings for resonance is equal to the value of the unknown capacitor. If a coil of known value is available, this can be used directly by connecting the unknown C across it and tuning the G.D.O. for resonance, transposing the above formula so that

• C=25,330

 $L \times f$.

Aid to Aerial Construction

Aerial checking can be carried out by coupling the G.D.O. as for a tuned circuit, but certain precautions have to be taken. A centre-fed dipole is current-fed on its fundamental frequency and thus the coupling point is shorted out and the G.D.O. coupled by proximity, or with a single turn loop. But on its second harmonic, the aerial is voltage-fed and half sections must be checked individually with the coupling point open-circuited. A single-ended aerial, such as a radio whip-type, is fed at the low impedance point; and the feeder is removed and replaced by a single-turn loop.

Constructing a multi-element array is aided by the G.D.O. by first coupling to the dipole and tun-

-continued on page 653



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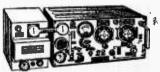
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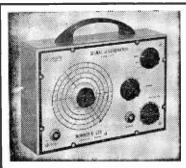
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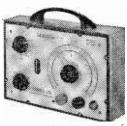
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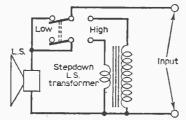
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Design for a Dual-Impedance Loudspeaker

A useful accessory for the workbench. By K. Berry

In the course of testing radios, television receivers and amplifiers, a general purpose loudspeaker is often needed for experimental purposes. Sometimes, a low impedance loudspeaker is required and at other times a high impedance instrument will be needed. On such occasions, it is usually necessary first to find a loudspeaker, also an output transformer and then to connect them together and to the equipment under test. This will always be a time consuming and tedious business and to overcome this problem, the author constructed a dual-impedance loudspeaker.

Fig. 1: The simple circuit arrangement of the unit.



The idea, which is very simple, is as follows. An ordinary low impedance extension loudspeaker was obtained, and an output transformer screwed securely inside the case. In the top of the case were fitted two terminals and a 2-pole change-over toggle switch.

The circuit is shown in Fig. 1, and the finished instrument in Fig. 2. The loudspeaker when thus modified, can be set for high or low impedance

operation at the turn of a switch.

The output transformer was one taken from an old radio receiver and matches 8.000Ω to 3Ω . It is

recommended that a transformer capable of carrying a primary current of about 50mA is used, as some equipments will pass such a current through the transformer.

Since, in this circuit, the voice coil of the loudspeaker is connected to the primary of the output transformer (when switched for high impedance operation), the loudspeaker chassis or

speaker chassis or frame could be at a high voltage with respect to earth, and accordingly care should be taken to ensure that accidental contact cannot be made with the loudspeaker chassis.

This device has proved to be such a great asset in testing and experimenting that the author wonders how he ever managed without one!

TEST GEAR TECHNIQUES

-continued from page 650

ing for resonant frequency. Then, without altering the G.D.O. setting, the additional elements can be added, spaced and adjusted for length until resonance is again obtained. One point worth mentioning is the effect of the earth on tuning. As the array is tuned relative to earth, adjustments should normally be made at the height above

Fig. 5: G.D.O. suitable for v.h.f. with bridge-connected d.c. amplifier for more accurate readings.

ground that it is intended to be used.

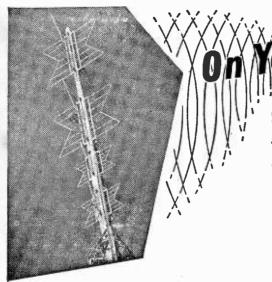
Fig. 2: The finished unit.

These are only a few of the more obvious applications of the G.D.O. A complete article could be devoted to its very versatile capabilities as signal generator and absorption type wavemeter. Various modifications and adaptations can be made to extend the range and sensitivity of the instrument.

Fig. 5 shows one such extension of the previous circuits, where a second valve is used as a d.c. amplifier with a bridge network to enable more

accurate reading to be obtained with loose coupling. Here, the valve functions as one arm of a bridge, with the potential developed across the G.D.O. grid leak applied to its grid. As this potential drops, the grid voltage becomes less negative and the resistance of the anode-cathode path decreases. This upsets the balance of the bridge and results in a good, positive indication. R5 is used to set the meter zero,

In conclusion, the author would like to thank those readers who have written, discussing the subject matter and occasionally pointing out discrepancies. It is regretted that sufficient space is not available to enter fully into the several questions that have arisen. Perhaps



FEEL compelled to give warning of dangers that may arise from the use of certain mains adaptors with battery type transistor receivers. How widespread this practice has become, I do not know, but I am aware of two recent cases of electrocution caused by transistor receivers operating from a.c. mains supplies through such devices.

In both tragedies, the adaptors were of foreign origin and it is all too obvious that neither of these meet the requirements laid down by British Standards Institute with respect to safety from

electric shock and fire.

Mr. J. Robson, of Newcastle, has recently drawn attention to one case of electrocution reported in the press, and he also forwarded a circuit diagram of a Japanese made mains operated power unit which he suspects to be of similar type to the unit involved in this fatality. On studying this diagram I find myself sharing the indignation expressed by this reader. That such a piece of apparatus should be made available to the general public without adequate instructions and warning concerning its use is little short of scandalous.

The unit referred to consists of a metal rectifier fed from the a.c. mains through a capacitor. The h.t. plus output line is separated from one side of

the a.c. mains only by a resistor.

Now a very dangerous state of affairs arises when this kind of power unit is connected up to a transistor portable receiver equipped, as so many are nowadays, with a socket for an external aerial and maybe a retractable rod aerial as well. In the majority of cases the aerial socket will be directly connected to the receiver h.t. plus line (signal 'earth')—but this presents no hazard when the receiver is powered by its normal internal battery. Should a mains operated power unit of the type just described be employed as substitute for the battery, the aerial circuit will then be connected to either the neutral or the line side of the mains, depending upon which way round the plug is fitted. There is thus a 50/50 chance that the aerial socket

our Wavelength By THERMION

(and, even more serious, the rod aerial) will be 'live' at the full mains voltage.

A Second Fatality Reported

Within a few weeks of receiving information concerning the above case I read of another fatal accident, where a youth was electrocuted in a bathroom. His death was attributed to a mains adaptor which was coupled to a transistor radio. A radio engineer giving evidence at the inquest stated that this particular adaptor (of German manufacture) would be regarded by many in the trade as potentially lethal. Now it was certainly wrong to use a mains powered receiver in a bath-room; frequent warnings are given about this and nobody should be in ignorance on this matter. But this cannot in any way excuse the makers, for if the facts as reported were correct, the power unit was inherently dangerous and had exposed metal which could readily become 'live'

I would urge all who have any dealings with devices of the nature to examine carefully each particular type that comes into their hands and satisfy themselves that the circuitry, components and mechanical construction are sufficiently sound for the proposed application; check especially that there is no risk of fire due to overheating nor any chance of 'live' parts being touched under normal

working conditions.

British Standards Safety Requirements

It is pertinent, finally, to mention some of the safeguards that are embodied in equipment conforming to BS415.

In this Standard certain requirements are laid down for 'non-isolated apparatus'—where direct connection is made between one side of the mains supply and any structural part of the apparatus. (A familiar example is, of course, the a.c./d.c. type receiver). It is stipulated that all terminals and sockets used for making external connections be effectively isolated from those parts of the circuit likely to be at mains potential. Good quality mica or paper dielectric capacitors of at least 750V working are specified for this purpose. In the case of receivers designed for use with an external aerial, the capacitor connected to the aerial socket must be shunted by a resistor of reasonably high value to prevent the accumulation of static charges on the aerial, because such charges could in time cause a breakdown in the isolating capacitor.

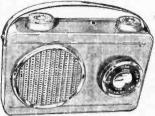
The apparatus should be housed in a cabinet or case of adequate strength and well insulated from the live parts. Any openings for ventilation must be of such a size as to prevent live parts within being touched by a finger. Control knobs must be securely fastened so that no portion of the metal spindles remains exposed; if grub screws are used, these must be well countersunk and, preferably, the holes sealed with an insulating substance.

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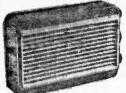
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DOUBLE-TRACE OSCILLOSCOPE

-continued from page 613

mentary lens, either of which can be purchased from a photographic dealer for a few shillings. A supplementary lens is designed for fixing immediately in front of the camera lens in the same way as a filter, and enables the lens to focus down to short distances.

"No. 3" lenses vary somewhat in power according to the manufacturer but a focusing table is available with the lens giving all necessary information. The data for a +3 diopter lens used with a normal type of 35mm. camera are as follows:

TABLE 4: SETTING-UP DATA FOR ±3 DIOPTER SUPPLEMENTARY LENS						
Camera Scale Reading	Distance from Lens front to Screen	Approximate Field Size				
3·5 ft.	10 in.	43/4 x 7 in.				
3 m.	25 cm.	12 x 18 cm.				
ω	13·1 in.	5 x 7½ in.				

If the camera has a focusing control it should be set at 3.5ft. or 3m., otherwise the " ∞ " figures can be used.

Special oscillograph film is available, but only in bulk quantities. However, it is quite possible to use whatever film happens to be in the camera at the time, using the exposures given in Table 5.

These values can only be approximate, as the setting of the "Intensity" control on the oscillo-

TABLE 5: AVERAGE EXPOSURE TIMES FOR AN APERTURE SETTING OF f/II

	Film Speed		[
BSI Scheiner	DIN	´ ASA Weston	Time
25°	15°	25	60 sec
32°	22°	125	15 sec
34°	24°	200	8 sec
37°	27°	400	4 sec

scope will have a considerable effect on the result. However, modern films provide quite a wide latitude for error.

With exposure times of this order, the camera cannot be held by hand, and a tripod (or a pile of books at the very least) will be necessary to support it during the exposure. If the camera is equipped with a cable release this should be used.

The actual exposure is best made in a darkened room or with the tube face screened from direct light, otherwise the oscillogram will lack contrast.

light, otherwise the oscillogram will lack contrast. If the camera has no "Time" exposure, it may be possible to bring the times given in Table 5 within the range of shutter speeds available on the camera by increasing the aperture of the lens (i.e. reducing its stop number). Here, the rule is to halve the exposure time for each stop by which the aperture is increased. If this is done, however, extra care will be needed in setting up the camera, as the depth of field will be that much less (a permissible error of about a quarter of an inch at f/3.5, as against more than an inch at f/11).

SHOWTIME ROUNDUP—continued

since they represent, in the main, the more popularly priced models and do not take in the majority of the more specialised manufacturers.

However, the new models seen showed a general improvement both technically and in presentation. With newer and better tape decks, higher quality audio circuits, more facilities and greater flexi-

bility, today's "popular" tape recorder represents extremely good value.

MAINS OPERATED RADIOS

Although there are proportionately few valve mains radio sets, some makers still keep them in production and a few new ones turned up at Showtime.

9	MAINS	OPERATED	RADIO -
Model	Wavebands	Price	Notes
EKCO U428	LW, MW, VHF	25 gns.	Push button pre-set tuning of up to fou VHF stations. Manual tuning for LW and MW
PHILIPS 417U	LW, MW, VHF	28 gns.	6 x 4" speaker.
4X23A	LW, MW, SW, VHF	37 gns.	Two 5" speakers, push-button tone control.
STELLA STI54U	LW, MW, VHF	27 gns.	6V, 6 x 4" speaker.
STI60A	LW, MW, SW, VHF	37 gns.	7V, two 5" dual-cone speakers.
UNITRA Goplana	LW, MW, SW, VHF	26½ gns.	Piano-key switching. Wood cabinet.
Alfa	MW, VHF	15 <u>1</u> gns.	Wood cabinet. 1.3W output.
Figaro 3	LW, MW, SW	9 gns.	1.5W output. Plastic cabinet. Wood cabine version, $9\frac{1}{2}$ gns.
Ramona	LW, MW, SW, VHF	26½ gns.	Unusual cabinet design.

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BY J. D. HASKELL

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Total output is 3W at better than 1% total distortion. Frequency response at maximum output 30—20kc/s better than ± 1dB. Hum and noise better than —80 dB at full output. Sensitivity with the loudness control in circuit is about 200 mV and this can be provided by any normal type pre-amplifier.

FOR enthusiasts who are satisfied with 3W of good quality, the following amplifier should suffice. The amplifier is good so far as stability, distortion and frequency response is concerned, and is adequate for all but the most discriminating listener.

The circuit is based upon three valves, these being a 6BR7, and EL84 and an EZ80. Precautions have been taken to ensure adequate valve life, and

maximum rating figures are never exceeded. The circuit has three negative feed-back loops; one of these is frequency selective, the other provides current feedback, and the third is a voltage feedback loop.

Loudness Control

Very few, if any, of the cheaper commercial amplifiers on the market have loudness controls.

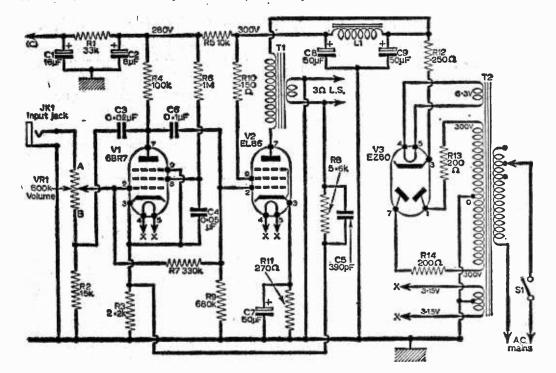


Fig. 1: The complete circuit diagram of the amplifier.

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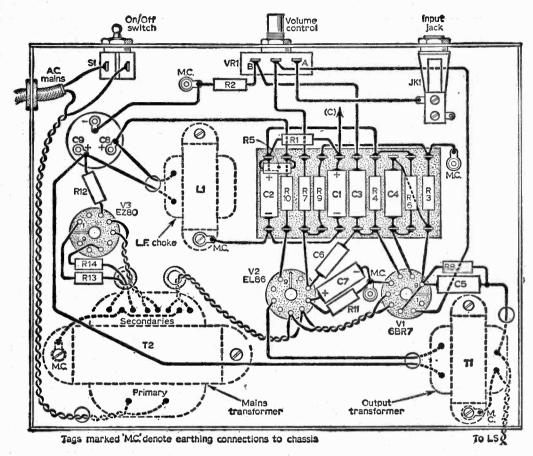


Fig. 2: A suggested layout for the amplifier.

In brief, this is a device which compensates for bass deficiency at low output levels. The loudness control functions as follows:

As the slider of the volume control is moved down towards "B", i.e. volume decreased, the amount of resistance in series with C3 is reduced and therefore more signal voltage is applied as negative feed-back to the grid. Due to the size of C3 the higher frequencies are readily passed—but very little at the lower frequencies.

H.F. Attenuation

This selective feedback results in attenuation of the high frequencies. It should now be clear that the boost is obtained at the expense of the high frequencies and hence adequate balance may be obtained by varying the setting of VR1. The resistor R2 prevents a short circuit to earth when the slider is at B. The values of C2 and R3 govern the frequency at which this control becomes effective. The adjustment of this control will be dealt with later on in this article.

Feedback

Some current feedback is applied at V1 by

omitting the normal cathode by-pass capacitor, and this gives a gradual low frequency rolloff and prevents the amplifier being overloaded at low frequencies. Some additional feedback is applied to the cathode of V1 from the output transformer secondary, via R8 and C5; the latter prevents high frequency ringing and instability and will suffice for any good quality output transformer. If a cheap type of output transformer is used a value of 1,000pF should prove suitable for C5. More feedback is applied to the grid of V1 from the grid of V2 via R7 and this keeps distortion at a minimum. The value of R4 has been chosen to give an essentially flat response up to at least 20kc/s.

Large Coupling Capacitor

The power handling capacity of an EL84 is well known, and hence a large coupling capacitor C6 was chosen to give an adequate bass response. It should also be remembered that if C6 were small in value a noticeable amount of transient distortion will occur due to phase lag in the capacitor. R11 should preferably be a 5% component.

	COMI	PONENTS L	.IST
Resisto	ors:	C8	50μF electrolytic 350V
RI	33k Ω R8 $\int 5.6$ k Ω 5% (for 3 Ω	LS) C9	50μF electrolytic 350V
R2	15k Ω 12k Ω 5% (for 15 Ω	LS) Transi	formers and choke:
R3 R4	2·2kΩ R9 680kΩ 100kΩ R10 150Ω 10kΩ R11 270Ω 3W	ΤI	Output transformer: Primary impedance $5k\Omega$; secondary 3Ω or 15Ω (Partridge
R5 R6 R7	IMΩ R12 250Ω 5W w.w. 330k 5% R13 200Ω IW R14 200Ω IW	Т2	P4073, or Parmeko P2661). Mains transformer: Tapped primary. Secondaries: 300-0-300V 8mA; 6-3V IA;
	All 10% , $\frac{1}{2}$ W carbon, except whotherwise stated.	here LI	6.3V (centre tapped) IA. Smoothing choke. 5H 75 Ω 60mA.
VRI	500 k Ω carbon potentiometer, log.	Valves	s:
C apaci CI		VI V2 V3	6BR7 EL86 EZ80
C2 C3	8μF electrolytic 350V 0·02μF paper 600V	Miscel	ilaneous:
C4 C5 C6 C7	0.05μF paper 600V 390pF ±10% silver mica 0.1μF paper 600V 50μF electrolytic 25V		Single pole on/off switch (S1). Input Jack and socket. Three B9A valveholders. One 10-way groupboard. Chassis 10in, x 8in, x 3in, approx.—(16s.w.g. aluminium.)

Output Transformer

Regarding the output transformer, no expense should be spared here, and the specified component should be bought if possible.

Adequate decoupling and smoothing is provided by C2, R5, C8 and C9, and hum is at least 80dB below full output. The resistors R13 and R14 are to limit the anode current on the plates of V3, but may be omitted, since the valve is working well within its maximum input rating.

A separate rectifier winding is preferable, though not essential, and if a common winding is to be used it should have a 2A rating. The heater winding in the circuit is centre-tapped to reduce the hum level, but again this could be of the ordinary variety without a centre tap and in this case one side of the winding should be earthed.

Wiring: Good wiring practice should be adhered to and all earth connections are to be made to a bus-bar, this being earthed at the input jack only. A suggested layout is given in Fig. 2. Setting up: After testing for any possible shortcircuits the mains can be applied and about 15 sec. should be allowed for the amplifier to warm up.

If you are using it in conjunction with a preamplifier the tap for the h.t. is taken from point C

in the circuit, about 10 mA is available.

The loudness control is turned to the maximum position and the volume control on the pre-amplifier is adjusted for normal listening level or, better still, for full output. The tone controls are now adjusted to match room acoustics. The preamplifier volume control should be left at that setting and the volume of the amplifier adjusted by means of the loudness control; adequate balance will be maintained down to about IW of output.

Summing up, the above amplifier will compare very well with the best on the market in this price bracket and should provide good quality and trouble-free performance when used with a good quality, correctly housed loudspeaker.

Audio Level Indicator

-continued from page 642

The signal supplied to the miniature loudspeaker was a 1,000c/s note obtained from a b.f.o. and recorded on tape, the output to the loudspeaker being in the order of 2W. A dB meter could be used to obtain exact figures of gain and loss.

The position of the loudspeaker and the micro-

phone when mounted on the rod differed very little but the reflected sound from the loudspeaker is masked due to the physical size of the instrument. If one is experimenting in this field of very interesting work it is well to remember that both the loudspeaker and microphone should face the umbrella reflector and not the sound.

Using the Noise Level Indicator Meter.

When the instrument has been completed and is ready for testing first switch on the instrument, then gently tap the microphone. The meter should give some indication by an upward movement. If the instrument is placed with the microphone facing a constant level audio signal the control VR1 can be rotated to give maximum reading.

The noise level indicator is very sensitive and will pick up a slight whisper at a few feet or more, so that when testing adjust the control VRI if necessary to prevent the meter pointer wrapping itself around the end stop.

If an external microphone is being used, remember to turn down the gain control on the indicator so that if the microphone happens to get sudden bang the meter will not suffer as a result.

The meter is not calibrated in terms of dB as this would necessitate the use of a decibel meter and a constant signal source, neither of which were available to the author. However, by experimenting a little with the results obtained the constructor will soon be able to use this instrument to a very surprising degree of accuracy in recording sound and setting up for steroe, etc.

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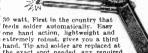
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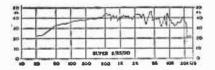
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SIR,—If carried to its logical conclusion your correspondent's views on democracy (October '63) would make life quite interesting, no driving tests, no pilots tickets, no building restrictions, perhaps all our problems would then be solved by the undenied right of the amateur physicist to test his home produced H-bomb (power limited to one megaton of course) in his own back yard.

With the arrival of this free radio age the present transistor portable craze among teenagers would be extended to transreceivers with the kids on high street all calling "CQ" to every blonde who

walks down the street.

Now as one of the initiated few who managed to pass the "highly technical examination" (I left school 26 years ago at the age of 14), I would like to point out to R.L.J. that if he so desires, and if he has the enthusiasm and willpower to spend a little time in study he too will not find it difficult to become one of the initiated few, otherwise my advice to R.L.J. is to take up bird watching or possibly politics. — C. M. Parry, GW3PHH, (Tonyrefail, Glam.)

PERMANENT VALVE IDENTIFICATION

S1R,—All amateur radio enthusiasts know the frustration of finding second-hand valves which, although probably mechanically sound, cannot be used because their type numbers have been removed by constant handling. Numerous remedies for this problem have been suggested in the past but none seem to be really permanent. However, I think I have found the answer by etching the number on to the valve envelope with acid.

I first cover a small area of the envelope with wax and then "write" the type number in the wax with a suitable stylus. Next I rub into the number just enough sodium fluoride to fill the depressions. Then I apply a couple of drops of concentrated sulphuric acid—which must be handled with the utmost care—and leave the valve undisturbed overnight. The wax can be removed the following morning, when the type number of the valve will be permanently etched on the envelope.—J. H. TURNER (Norwich).

CORRESPONDENTS WANTED

S1R,—A friend and I, aged 12 and 14 years respectively, would like to correspond with other readers of P.W. who are about the same age. We are keen S.W.L.s and are already interested in many aspects of radio and electronics and would therefore be pleased to hear from any young readers of P.W. having similar interests.— P. GASKELL, 131 Greenfield Road, St. Helens, Lancs.

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELEPHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of the cover.

The Editor does not necessarily agree with the opinions expressed by his correspondents

Sir,—I would be grateful if any reader could sell or loan me . . .

September and October 1958, the August, September and October 1959, and the February and December 1962 issues of P.W.—J. R. AULT, 17, Hollyhedge Road, West Bromwich, Staffs.

issues of P.W.—P. Warren, 6 Lime Grove, St. Neots, Huntingdonshire.

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... the circuit and/or manual for the Hallicrafters S-40B receiver.—M. J. WICKSTEAD, 99 Earlsfield Road, London SW18.

... the June and August 1961 and May 1963 issues of P.W.—M. HERRING, 59 Groundwell Road, Swindon, Wilts.

... the August 1962 issue of P.W.—D. DAVIDSON, c/o Clark, 43 Acrehill Street, Glasgow

... the circuit diagram of a threewaveband H.M.V. receiver, type 482. — P. K. TARLING, 9 Guithavon Street, Witham, Essex.

the No. 19 set and any other information available.—J. SCANLAN, 22 Sidland Road, Barmulloch, Glasgow N1.

... the circuit and wiring diagram of the No. 19 set supply unit No. 2.—D. R. BROOKS, 61 Elmsleigh Gardens, Bassett, Southampton.

... the issues of P.W. containing information on the R.1155 receiver.—W. DAVIES, 78 Lapwing Lane, Brinnington, Stockport, Cheshire.

... a service sheet for the Sharp transistor receiver, model No. BX-326.—G. STEWART, 12 Baronhill, Cumbernauld, Glasgow.

... the April 1953 issue of P.W.—A. J. HILLS, 89 Cornwallis Road, Cowley, Oxford.

TREMOLO OR VIBRATO

SIR,—There seems to be some confusion in the minds of some of the contributors to your magazine, with regard to the use of the term "tremolo unit" in describing various devices associated with guitar amplifiers and electronic organs. The confusion seems to arise from a misinterpretation of the musical terms tremolo and vibrato.

-continued overleaf



held on the 2nd.

ISLE OF WIGHT RADIO SOCIETY
Hon. Sec.: Capt. E. C. Dolling, "Sweet Briars", New Road,
Wootton Bridge, I.W.

At recent meetings members have been preparing for the increased activity which the approaching winter months will bring. Now that the Society has obtained its own callisign, all efforts are being made to get on the air as soon as possible from their new premises of the Unity Hall, Wootton Bridge.

LOUGHTON AND DISTRICT RADIO CLUB Hon. Sec.: D. J. Penny, G3PEN, 175 Burrow Road, Chigwell,

This Club has only recently been formed and at the moment members meet fortnightly at the Loughton Community Centre, Debden, Essex. Separate meetings are held for youngar members when instruction on radio theory and morse is given.

MELTON MOWBRAY AMATEUR RADIO SOCIETY Hon. Sec.: D. W. Lilley, G3FDF, 23 Melton Road, Asfordby Hill, Melton Mowbray, Leicestershire.
On the 19th September the Annual General Meeting of this Society was held in Melton Mowbray. The main item on the agenda was the programme of activities for the winter session, which was discussed and compiled during the evening.

MITCHAM AND DISTRICT RADIO SOCIETY
Hoa. Sec.: Alan Thurley, 50 Bruce Road, Mitcham, Surrey.
On 13th September a junk sale was held at the Society's H.Q.
The Society is making preparations to co-operate with the
Mitcham District Scouts in the forthcoming Boy Scouts "Jamboreeon-the-Air" which will be held in October. Members for the
Society will be operating equipment on the h.f. and 2m bands
during this two-day event.

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sac.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

On 11th September Northern Heights members were hosts On The September 1 Northern reights of the Manchester Radio Society for a Pea and Pie Supper. Later in the month on the 25th, K. Walton (G3IKS) gave a lecture on "Lightning", explaining its nature and effects. G3IKS illustrated his lecture with dramatic demonstrations using a † million volt discharge to produce some considerable "flashes".

Preparations are going ahead to organise a coach party of 40 to visit this year's International Communications Exhibition.

as shown above

READING AMATEUR RADIO CLUB Hon. Sec.: R. G. Nash, G3EJA, "Peacehaven", 9 Holybrook

Road, Reading, Berkshire.

The only meeting for September was held on the 28th when "Transistor Power Supplies" was the subject of the lecture given by GRSC.

SCARBOROUGH AMATEUR RADIO SOCIETY
Hen. Sec.: P. B. Briscombe, G8KU, "Rosescre", Irton,
Scarborough, Yorkshire.
The month's activities began with a sale of surplus gear on 15th
September. On the 12th members made "at home" visits to
G8KU, C3NRI, G3NRS and G3JTG.
A week later, "Antennas and Couplers" was the topic under

examination, and on the 26th a quiz provided the evening's enter-

SHEFFIELD AMATEUR RADIO CLUB Hon. Sec.: D. A. Justice, G3PYL, 314 Stannington Road,

Sheffield 6. The Club meets on every second and fourth Friday in the month when new members will be welcomed. Members and prospective members are asked to note the new address of the Club secretary

WESSEX AMATEUR RADIO GROUP Hon. Sec.: G. J. Fowle, 138 Surrey Road, Branksome, Pools,

It is intended to record all the Group's activities this year on mm. colour cine film.

On 12th September members visited Pool power station and on the 16th an informal get-together was held at the President's house.

At the last meeting for the month, members took part in a quiz and also heard a talk on "Railway Signalling and Communications" which was given by G. J. Fowle.

WEST KENT AMATEUR RADIO SOCIETY

Members operated a 2m station for 24 hours when V.H.F. National Field Day was held on 7/8th September.
The second meeting for the month was devoted to the first of a series of talks and discussions entitled "100 Years of Wireless".

WIMBLEDON AND DISTRICT RADIO SOCIETY
Hon. Sec.: R. G. Baker, G6QN, I Boundary Road, Colliers
Wood, Lendon S.W.19.

This society has recently been re-established, after a considerable number of years, by the efforts of a small body of local enthusiasts.

Number of years, by the emorts of a small body of local entitudents. A pro-tem committee will continue to function until December, when a properly constituted panel of officers will be elected.

Local radio enthusiasts are invited to attend any of the meetings which are held on the second friday of each month at the Community Centre, St. George's Road, Wimbledon, London S.W.19.

WIRRAL AMATEUR RADIO SOCIETY Hon. Sec.: A. Seed, G3FOO, 31 Withert Avenue, Bebington, Wirral, Cheshire.

September activities began with e sale of surplus equipment. This was followed by a talk on "Valve Uses", given on the 18th.
The first meeting in October was the Annual General Meeting,

R.S.G.B. Contests for October. R.A.E.N. Raily (6th October); 7Mc/s DX Contest—phone (19th to 20th October) and Second 420Mc/s Contest (27th October).

Correction. We draw the attention of readers to the fact that the South Shields and District Amateur Radio Club's Mobile Rally, which was reported on the September Club News page as having been held on 7th July, did not, in fact, take place, due to an unforeseen incident.

LETTERS TO THE EDITOR

-continued from previous page

The tremolo effect describes the slight variations of frequency which may be produced by an in-strument to add "colour" to an otherwise steady note and is, in fact, frequency modulation of the note. The vibrato effect, however, describes the variations in amplitude which may be produced, and is, in fact, amplitude modulation of the note.

The tremolo effect is produced mechanically in the case of a guitar, by changing the tension in the strings by means of a lever and spring system, commonly called a "tremolo arm". The vibrato effect is usually produced electronically in the amplifier system by some sort of amplitude modulator such as described in the March 1963 issue of P.W. In the case of electronic organs both effects may be produced by modulating the oscillators producing the fundamental notes.

The devices described in Practical Wireless for use with guitar amplifiers are amplitude modulation devices and the term "tremolo unit although used by some manufacturers to describe these units, is quite incorrect and misleading. These devices are "vibrato units". I for one would be very interested to see an electronic device which produces a true tremolo effect with guitar amplifiers!—Peter A. Roe (Aspley, Nottingham).

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NEWNES

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-continued from page 633 and rotate the oscillator coil and IFT cores until they are about level with the tops of the screening

With the volume control advanced about one quarter, as mentioned, try to tune in the local station. If it is heard, tune it in as well as possible, and adjust the 1FT cores for best volume. Signals may become much too loud, in which case the volume control should be turned back.

It should then be possible to tune in some transmission near the high frequency (low wavelength) end of the band; that is, with the variable capacitor nearly open. Rotate the trimmers to bring this

transmission up to best volume.

A station of high wavelength (capacitor nearly closed) is then sought. The aerial winding is then pushed along the ferrite rod, to bring this up to best volume.

Repeating the procedure once or twice, with weak signals, should give correct ganging, as shown by full sensitivity throughout the whole tuning range.

If the local station cannot in any circumstances be heard, attach a few feet of wire, as an external aerial, to the green lead tag. This should give a signal allowing rough adjustments to be made. It should then be possible to hear the station with no external aerial, and alignment can then proceed as mentioned.

Adjustment to this part of the receiver will remain approximately correct, even when the other stages are added. In view of the simple nature of the circuit, no particular difficulty should arise in aligning. The most probable faults are wrong band coverage.

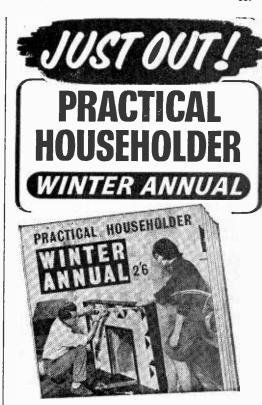
If the set does not tune to a high enough wavelength, even with the capacitor fully closed, this can be corrected by screwing the oscillator coil in slightly, and pushing the aerial winding a little

farther on the rod.

Should the receiver fail to reach a low enough wavelength, with the tuning capacitor fully open, this indicates that the trimmers are screwed down too far. Unscrew both by an equal amount, then re-trim as explained.

TO BE CONTINUED

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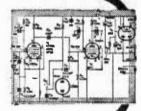
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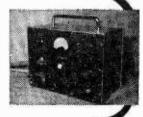
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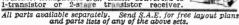


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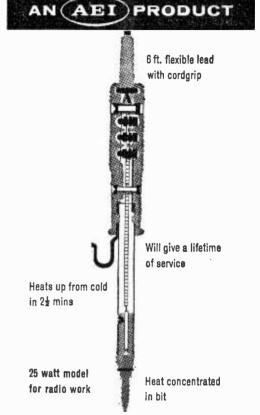
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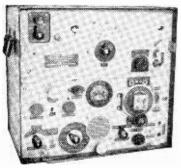
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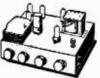
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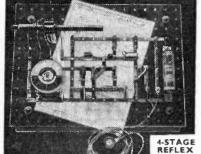
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